



ITTC Symbols and Terminology List

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Updated by the 28th ITTC Quality Systems Group

ITTC Symbols and Terminology List, Version 2017

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| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

1. GENERAL

1.1 Fundamental Concepts

1.1.1 Uncertainty

(The following table follows ISO/IEC Guide 98-3:2008 – Annex J)

| | | | | |
|-----------------------------|--|--|--|---|
| a | | Half-width of a rectangular distribution | Half-width of a rectangular distribution of possible values of input quantity X_i : $a = (a_+ - a_-) / 2$ | |
| a_+ | | Upper bound | Upper bound, or upper limit, of input quantity X_i : | |
| a_- | | Lower bound | Lower bound, or lower limit, of input quantity X_i : | |
| b_+ | | Upper bound of the deviation | Upper bound, or upper limit, of the deviation of input quantity X_i from its estimate x_i : $b_+ = a_+ - x_i$ | |
| b_- | | Lower bound of the deviation | Lower bound, or lower limit, of the deviation of input quantity X_i from its estimate x_i : $b_- = x_i - a_-$ | |
| c_i | | Sensitivity coefficient | $c_i = \partial f / \partial x_i$. | 1 |
| f | | Function | Functional relationship between measurand Y and input quantities X_i on which Y depends, and between output estimate y and input estimates x_i on which y depends. | 1 |
| $\partial f / \partial x_i$ | | Partial derivative | Partial derivative of f with respect to input quantity x_i | 1 |
| k | | Coverage factor | For calculation of expanded uncertainty $U = k u_c(y)$ | 1 |
| k_p | | Coverage factor for probability p | For calculation of expanded uncertainty $U_p = k_p u_c(y)$ | 1 |
| n | | Number of repeated observations | | 1 |
| N | | Number of input quantities | Number of input quantities X_i on which the measurand Y depends | 1 |
| p | | Probability | Level of confidence: $0 \leq p \leq 1.0$ | 1 |
| q | | Random quantity | | 1 |
| \bar{q} | | Arithmetic mean or average | | 1 |
| q_k | | k th observation of q | k th independent repeated observation of randomly varying quantity q | 1 |
| $r(x_i, x_j)$ | | Estimated correlation coefficient | $r(x_i, x_j) = u(x_i, x_j) / (u(x_i) u(x_j))$ | 1 |
| s_p^2 | | Pooled estimate of variance | | 1 |
| s_p | | Pooled experimental standard deviation | Positive square root of s_p^2 | 1 |
| $s^2(\bar{q})$ | | Experimental variance of the mean | $s^2(\bar{q}) = s^2(q_k) / n$; estimated variance obtained from a Type A evaluation | 1 |
| $s(\bar{q})$ | | Experimental standard deviation of the mean | Positive square root of $s^2(\bar{q})$ | 1 |
| $s^2(q_k)$ | | Experimental variance from repeated observations | | 1 |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|---------------------------|-----------------|---|---|---------|
| $s(q_k)$ | | Experimental standard deviation of repeated observations | Positive square root of $s^2(q_k)$ | 1 |
| $s^2(\bar{X}_i)$ | | Experimental variance of input mean | From mean \bar{X}_i , determined from n independent repeated observations $X_{i,k}$, estimated variance obtained from a Type A evaluation. | 1 |
| $s(\bar{X}_i)$ | | Standard deviation of input mean | Positive square root of $s^2(\bar{X}_i)$ | 1 |
| $s(\bar{q}, \bar{r})$ | | Estimate of covariance of means | | 1 |
| $s(\bar{X}_i, \bar{X}_j)$ | | Estimate of covariance of input means | | 1 |
| $t_p(v)$ | | Inverse Student t | Student t -distribution for v degrees of freedom corresponding to a given probability p | 1 |
| $t_p(v_{\text{eff}})$ | | Inverse Student t for effective degrees of freedom | Student t -distribution for v_{eff} degrees of freedom corresponding to a given probability p in calculation of expanded uncertainty U_p | 1 |
| $u^2(x_i)$ | | Estimated variance | Associated with input estimate x_i that estimates input quantity X_i | 1 |
| $u(x_i)$ | | Standard deviation | Positive square root of $u^2(x_i)$ | 1 |
| $u(x_i, x_j)$ | | Estimated covariance | | 1 |
| $u_c^2(y)$ | | Combined variance | Combined variance associated with output estimate y | 1 |
| $u_c(y)$ | | Combined standard uncertainty | Positive square root of $u_c^2(y)$ | 1 |
| $u_{cA}(y)$ | | Combined standard uncertainty from Type A | From Type A evaluations alone | 1 |
| $u_{cB}(y)$ | | Combined standard uncertainty from Type B | From Type B evaluations alone | 1 |
| $u_c(y_i)$ | | Combined standard uncertainty | Combined standard uncertainty of output estimate y_i when two or more measurands or output quantities are determined in the same measurement | 1 |
| ${}_i u_i^2(y)$ | | Component of combined variance | ${}_i u_i^2(y) \equiv [c_i u(x_i)]^2$ | 1 |
| ${}_i u_i(y)$ | | Component of combined standard uncertainty | ${}_i u_i(y) \equiv c_i u(x_i)$ | 1 |
| $u(x_i)/ x_i $ | | Relative standard uncertainty of output estimate x | | 1 |
| $u_c(y)/ y $ | | Relative combined standard uncertainty of output estimate y | | |
| $[u(x_i)/ x_i]^2$ | | Estimated relative variance | Estimated relative variance associated with input estimate x_i | |
| $[u_c(y)/ y]^2$ | | Relative combined variance | Relative combined variance associated with output estimate y | |
| $u(x_i, x_j)/ x_i x_j $ | | Estimated relative covariance | Estimated relative covariance associated with input estimates x_i and x_j | |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|--------------------|-----------------|---|---|---------|
| U | | Expanded uncertainty | Expanded uncertainty of output estimate y that defines an interval $Y = y \pm U$ having a high level of confidence, equal to coverage factor k times the combined standard uncertainty $u_c(y)$ of y : $U = k u_c(y)$ | |
| U_p | | Expanded uncertainty associated to confidence level p | Expanded uncertainty of output estimate y that defines an interval $Y = y \pm U_p$ having a high level of confidence p , equal to coverage factor k_p times the combined standard uncertainty $u_c(y)$ of y : $U_p = k_p u_c(y)$ | |
| x_i | | Estimate of input quantity X_i | Estimate of input quantity X_i NOTE when x_i is determined from the arithmetic mean or average of n independent repeated observation $x_i = \overline{X}_i$ | |
| X_i | | i^{th} input quantity | i^{th} input quantity on which measurand Y depends NOTE X_i may be the physical quantity or the random variable | |
| \overline{X}_i | | Estimate of the value of input quantity X_i | Estimate of the value of input quantity X_i equal to the arithmetic mean or average of n independent repeated observation $X_{i,k}$ of X_i | |
| $X_{i,k}$ | | k^{th} independent repeated observation of X_i | | |
| y | | Estimated of measurand Y or Result of a measurement or Output estimate | | |
| y_i | | Estimate of measurand Y_i | Estimate of measurand Y_i when two or more measurands are determined in the same measurement | |
| Y | | A measurand. Estimated relative uncertainty of standard uncertainty $u(x_i)$ of inputs estimate x_i | | |
| μ_p | | Expectation or mean of the probability distribution | Expectation or mean of the probability distribution of random-varying quantity q | |
| ν | | Degrees of freedom (general) | | |
| ν_i | | Degrees of freedom | Degrees of freedom, or effective degrees of freedom of standard uncertainty $u(x_i)$ of input estimate x_i | |
| ν_{eff} | | Effective degrees of freedom | Effective degrees of freedom of $u_c(y)$ used to obtain $t_p(\nu_{\text{eff}})$ for calculating expanded uncertainty U_p | |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|------------------------|-----------------|---|---|---------|
| σ^2 | | Variance of a probability | Variance of a probability distribution of (for example) a randomly-varying quantity q , estimated by $s^2(q_k)$ | |
| σ | | Standard deviation of a probability distribution | Standard deviation of a probability distribution, equal to the positive square root of σ^2 | |
| $\sigma^2(\bar{q})$ | | Variance of \bar{q} | Variance of \bar{q} , equal to σ^2/n , estimated by $s^2(\bar{q}) = \frac{s^2(\bar{q}_k)}{n}$ | |
| $\sigma(\bar{q})$ | | Standard deviation of \bar{q} | Standard deviation of \bar{q} , equal to the positive root of $\sigma^2(\bar{q})$ | |
| $\sigma^2[s(\bar{q})]$ | | Variance of experimental standard deviation $s(\bar{q})$ of \bar{q} | | |
| $\sigma[s(\bar{q})]$ | | Standard deviation of experimental standard deviation $s(\bar{q})$ of \bar{q} , equal to the positive square root of $\sigma^2[s(\bar{q})]$ | | |

1.1.2 Coordinates and Space Related Quantities

Orientation of coordinates

A problem of general interest, the orientation of the axes of coordinate systems, has been treated extensively in the Report of the 17th ITTC Information Committee. The present QS Group recommends that the orientations of the coordinate systems chosen for convenience should be stated explicitly in any case. The coordinate system orientation should not be inferred from the symbols and/or names of the concepts or from national or professional traditions. All sign conventions of related Quantities should be consistent with the orientation chosen.

For ready reference the recommendation of the 17th ITTC Information Committee is quoted in the following.

"In order to adapt ITTC nomenclature to common practice a proposal for a standard coordinate system was published in the newsletter No 7, March 1983, to generate discussion. The response was quite diverse. On the one hand it was suggested that instead of the two orthogonal right handed systems with the positive x-axis forward and the positive z-axis either up- or downward as proposed only one system should be selected, in particular the one with the positive z-axis upwards. On the other hand the attention of the Information Committee was drawn to the fact that in ship flow calculations neither of the two systems proposed is customary. Normally the x-axis is directed in the main flow direction, i.e. backwards, the y-axis is taken positive to starboard and the z-axis is positive upwards. The origin of the co-ordinates in this case is usually in the undisturbed free surface half way between fore and aft perpendicular.

In view of this state of affairs the Information Committee (now Quality System Group - QSG) may offer the following recommendation, if any:

Axes, coordinates

Preferably, orthogonal right handed systems of Cartesian co-ordinates should be used, orientation and origin in any particular case should be chosen for convenience.

Body axes (x, y, z)

Coordinate systems fixed in bodies, ocean platforms, or ships.

For the definition of hull forms and ocean wave properties and the analysis of structural deflections it is customary to take the x-axis positive forward and parallel to the reference or base line used to describe the body's shape, the y-axis positive to port, and the z-axis positive upwards.

For seakeeping and manoeuvrability problems the coordinate system is defined as follows: usually the x-axis as before the y-axis positive to starboard, and the z-axis positive downwards, the origin customarily at the centre of mass of the vehicle or at a geometrically defined position.

For ship flow calculations usually the x-axis positive in the main flow direction, i.e. backwards, the y-axis positive to starboard, and the z-axis positive upwards, the origin customarily at the intersection of the plane of the undisturbed free-surface, the centre plane, and the mid-ship section.

Fixed or space axes (x_0, y_0, z_0)

Coordinate systems fixed in relation to the earth or the water. For further references see ISO Standard 1151/1 ...6: Terms and symbols for flight dynamics.

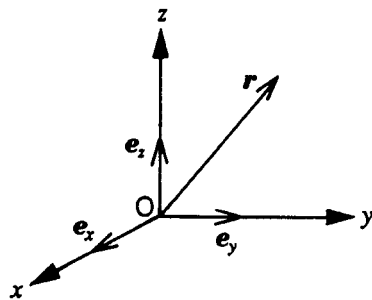
There may be other coordinate systems in use and there is no possibility for the adoption of a single system for all purposes. Any problem requires an adequate coordinate system and transformations between systems are simple, provided that orientations and origins are completely and correctly documented for any particular case."

Origins of coordinates

In sea keeping and manoeuvrability problems customarily the centre of mass of the vehicle is chosen as the origin of the coordinates. This is in most cases not necessarily advantageous, as all the hydrodynamic properties entering the problems are related rather to the geometries of the bodies under investigation. So any geometrically defined point may be more adequate for the purposes at hand.

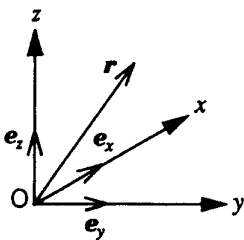
ISO Standard 31-11 makes the following suggestions

| Item No. | Coordinates | Position vector and its differential | Name of coordinate system | Remarks |
|--|-------------------------|---|---------------------------|---|
| 11-12.1 (-) | x, y, z | $\mathbf{r} = x\mathbf{e}_x + y\mathbf{e}_y + z\mathbf{e}_z$ $d\mathbf{r} = dx\mathbf{e}_x + dy\mathbf{e}_y + dz\mathbf{e}_z$ | cartesian coordinates | $\mathbf{e}_x, \mathbf{e}_y$ and \mathbf{e}_z form an orthonormal right-handed system. See Figure 1. |
| 11-12.2 (-) | ρ, φ, z | $\mathbf{r} = \rho\mathbf{e}_\rho + z\mathbf{e}_z$ $d\mathbf{r} = d\rho\mathbf{e}_\rho + d\varphi\mathbf{e}_\varphi + dz\mathbf{e}_z$ | cylindrical coordinates | $\mathbf{e}_\rho(\varphi), \mathbf{e}_\varphi(\varphi)$ and \mathbf{e}_z form an orthonormal right-handed system. See Figures 3 and 4. If $z = 0$, then ρ and φ are the polar coordinates |
| 11-12.3 (-) | r, ϑ, φ | $\mathbf{r} = r\mathbf{e}_r$ $d\mathbf{r} = dr\mathbf{e}_r + r d\vartheta\mathbf{e}_\vartheta + r \sin \vartheta d\varphi\mathbf{e}_\varphi$ | spherical coordinates | $\mathbf{e}_r(\vartheta, \varphi), \mathbf{e}_\vartheta(\vartheta, \varphi)$ and $\mathbf{e}_\varphi(\varphi)$ form an orthonormal right-handed system. See Figures 3 and 5. |
| NOTE 1 If, exceptionally, a left-handed system (see figure 2) is used for certain purposes, this shall be clearly stated to avoid the risk of sign errors. | | | | |



The x-axis is pointing towards the viewer.

Figure 1 — Right-handed cartesian coordinate system



The x-axis is pointing away from the viewer.

Figure 2 — Left-handed cartesian coordinate system

1.

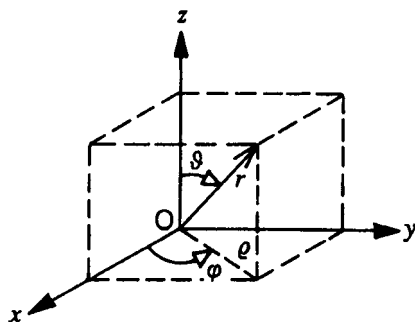


Figure 3 — Oxyz is a right-handed coordinate system

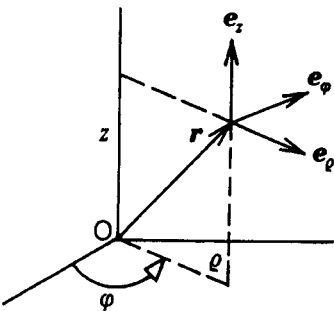


Figure 4 — Right-handed cylindrical coordinates

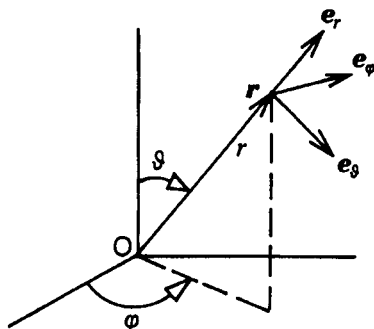


Figure 5 — Right-handed spherical coordinates

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

1.1.2.1 Basic Quantities

| | | | | |
|---|-------------------------------------|---|--|---|
| s | S | Any scalar quantity distributed, maybe singularly, in space | $\int ds$ | |
| S_{ij}^0 | SM0(I,J) | Zero th order moment of a scalar quantity | $\int \delta_{ij} ds = \delta_{ij} S$ | |
| S_{ij}^1 | SM1(I,J) | First order moment of a scalar quantity, formerly static moments of a scalar distribution | $\int \epsilon_{ikj} x_k ds$ | |
| S_{ij}^2 | SM2(I,J) | Second moment of a scalar quantity, formerly moments of inertia of a scalar distribution | $\int \epsilon_{kli} x_l \epsilon_{jkm} x_m ds$ | |
| S_{uv} | S(U,V) | Generalized moment of a scalar quantity distributed in space | $S_{ij} = S_{ij}^0$ $S_{i, 3+j} = S_{ij}^{1,T}$ $S_{3+i, j} = S_{ij}^1$ $S_{3+i, 3+j} = S_{ij}^2$ | |
| T_{ij} | T(I,J) | Tensor in space referred to an orthogonal system of Cartesian coordinates fixed in the body | $T_{ij}^s + T_{ij}^a$ | |
| T_{ij}^A | TAS(I,J) | Anti-symmetric part of a tensor | $(T_{ij} - T_{ji}) / 2$ | |
| T_{ij}^S | TSY(I,J) | Symmetric part of a tensor | $(T_{ij} + T_{ji}) / 2$ | |
| T_{ij}^T | TTR(I,J) | Transposed tensor | T_{ji} | |
| $T_{ij} v_j$ | | Tensor product | $\Sigma T_{ij} v_j$ | |
| u_i, v_i | U(I), V(I) | Any vector quantities | | |
| $u_i v_i$ | UVPS | Scalar product | $u_i v_i$ | |
| $u_i v_j$ | UVPD(I,J) | Diadic product | $u_i v_j$ | |
| $u \times v$ | UVPV(I) | Vector product | $\epsilon_{ijk} u_j v_k$ | |
| V_{0i}, V_i | V0(I), V(I) | Zeroth order moments of a vector quantity distributed in space, referred to an orthogonal system of Cartesian coordinates fixed in the body | $\int dv_i$ | |
| V_i^1 | V1(I) | First order moments of a vector distribution | $\int \epsilon_{ijk} x_j dv_k$ | |
| V_u | V(U) | Generalized vector | $V_i = V_{0i}^0$ $V_{3+i} = V_i^1$ | |
| x, x_1 y, x_2 z, x_3 | X, X(1) Y, X(2) Z, X(3) | Body axes and corresponding Cartesian coordinates | Right-hand orthogonal system of coordinates fixed in the body | m |
| x_0, x_{01} y_0, x_{02} z_0, x_{03} | X0, X0(1) Y0, X0(2) Z0, X0(3) | Space axes and corresponding Cartesian coordinates | Right-hand orthogonal system of coordinates fixed in relation to the space | m |
| x_F, x_{F1} y_F, x_{F2} z_F, x_{F3} | XF, XF(1) YF, XF(2) ZF, XF(3) | Flow axes and corresponding Cartesian coordinates | Right-hand orthogonal system of coordinates fixed in relation to the flow | m |
| ϵ_{ijk} | EPS(I,J,K) | Epsilon operator | $+1 : ijk = 123, 231, 312$ $1 : ijk = 321, 213, 132$ $0 : \text{if otherwise}$ | |
| δ_{ij} | DEL(I,J) | Delta operator | $+1 : ij = 11, 22, 33$ $0 : \text{if otherwise}$ | |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

1.1.3 Time and Frequency Domain Quantities

1.1.3.1 Basic Quantities

| | | | | |
|-------|-------|---|---|-----|
| a | ADMP | Damping | s^r , in Laplace variable | 1/s |
| f | FR | Frequency | | Hz |
| f_c | FC | Basic frequency in repeating functions | $1 / T_c$ | Hz |
| f_s | FS | Frequency of sampling | $1 / T_s$ period in repeating spectra | Hz |
| i | I | Imaginary unit | sqrt(-1) | 1 |
| I | IM | Imaginary variable | | 1 |
| j | J | Integer values | $-\infty \dots +\infty$ | 1 |
| R | R | Complex variable | $\exp(s T_s)$ Laurent transform | |
| s | S | Complex variable | $a + 2\pi i f$ Laplace transform | 1/s |
| t | TI | Time | $-\infty \dots +\infty$ | s |
| t_j | TI(J) | Sample time instances | $j T_s$ | |
| T_c | TC | Period of cycle | $1 / f_c$ duration of cycles in periodic, repeating processes | s |
| T_s | TS | Period of sampling | Duration between samples | s |
| x | x | Values of real quantities | $x(t)$ | |
| X | | Real "valued" function | | |
| x_j | X(J) | Variables for samples values of real quantities | $x(t_j) = \int x(t) \delta(t - t_j) dt$ | |
| z | Z | Complex variable | | |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
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1.1.3.2 Complex Transforms

| | | | | |
|----------|--------|--|---|--|
| x^A | XA | Analytic function | $X^A(t) = X(t) + iX^H(t)$ | |
| x^{DF} | XDF | Fourier transform of sampled function | $X^{DF}(f) = \sum x_j \exp(-i2\pi f j T_s)$ i.e. periodically repeating $= X(0)/2 + \sum f_s X^F(f + j f_s)$ sample theorem: aliasing! | |
| x^{DL} | XDL | Laurent transform of sampled function | $X^{DL}(s) = \sum x_j \exp(-s j T_s)$ | |
| x^F | XFT | Fourier transform | $X^F(f) = \int X(t) \exp(-i2\pi f t) dt$ inverse form: $= \int X^F(f) \exp(-i2\pi f t) dt$ if $X(t) = 0$ and $a = 0$ then $X^F(f) = X^L(f)$ | |
| x_j^F | XFT(J) | Fourier transform of periodic function | $1/T_C \int X(t) \exp(-i2\pi j t/T_C) dt$ $t = 0 \dots T_C$ $X^F = \sum x_j^F \delta(f - j/T_C)$ inverse form: $X(t) = \sum x_j^F \exp(-i2\pi j t/T_C)$ | |
| x^H | XHT | Hilbert transform | $X^H(t) = 1/\pi \int X(\tau)/(t - \tau) d\tau$ | |
| x^{HF} | XHF | Fourier transform of Hilbert transform | $X^{HF}(f) = X^F(f)(-i \operatorname{sgn} f)$ $(1/t)^F = -i \operatorname{sgn} f$ | |
| x^L | XLT | Laplace transform | $X^L(s) = \int X(t) \exp(-st) dt$ if $X(t < 0) = 0$ then $= (X(t) \exp(-at))^F$ | |
| x^R | XRT | Laurent transform | $X^R(r) = \sum x_j r^{-j} = X^{DL}$ | |
| x^S | XS | Single-sided complex spectra | $X^S(f) = X^F(f)(1 + \operatorname{sgn} f)$ $= X^{AF}$ i.e. $= 0$ for $f < 0$ | |
| x_j^S | XS(J) | Single-sided complex Fourier series | $X_j^F(1 + \operatorname{sgn} j)$ line spectra | |

1.1.3.3 Complex Quantities

| | | | | |
|-------|-----|-----------------------------|--|--|
| z^a | ZAM | Amplitude | $\operatorname{mod}(z) = \sqrt{z^r{}^2 + z^i{}^2}$ | |
| z^c | ZRE | Real or cosine component | $z^c = \operatorname{real}(z) = z^a \cos(z^p)$ | |
| z^i | ZIM | Imaginary or sine component | $\operatorname{imag}(z) = z^a \sin(z^p) = z^s$ | |
| z^j | ZCJ | Conjugate | $z^r - i z^i$ | |
| z^l | ZLG | (Phase) Lag | | |
| z^p | ZPH | Phase | $\operatorname{arc}(z) = \arctg(z^i / z^r)$ | |
| z^r | ZRE | Real or cosine component | $\operatorname{real}(z) = z^a \cos(z^p) = z^c$ | |
| z^s | ZIM | Imaginary or sine component | $z^s = \operatorname{imag}(z) = z^a \sin(z^p)$ | |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
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1.1.4 Random Quantities and Stochastic Processes

1.1.4.1 Random Quantities

| | | | | |
|---------------------------|--------------|---|--|---|
| g^E, g^M, g^{MR} | GMR | Expected value of a function of a random quantity | $E(g) = \int g(x)f_x(x)dx$ $x = -\infty \dots \infty$ | |
| x, y | X, Y | Random quantities | $x(\zeta), y(\zeta)$ | |
| x_i, y_i | $X(I), Y(I)$ | Samples of random quantities | $i = 1 \dots n$ n : sample size | |
| $(x^m)^E$ | $XmMR$ | m -th moment of a random quantity | $(x^m)^E$ | |
| x^D, x^{DR}, σ_x | XDR | Standard deviation of a random quantity | $x^{VR \ 1/2}$ | |
| x^{DS}, s_x | XDS | Sample deviation of a random quantity | $x^{VS \ 1/2}$, unbiased random estimate of the standard deviation | |
| xx^R, xx^{MR}, R_{xx} | XXMR | Auto-correlation of a random quantity | $x x^E$ | |
| xy^R, xy^{MR}, R_{xy} | XYMR | Cross-correlation of two random quantities | $x y^E$ | |
| x^E, x^M, x^{MR}, μ_x | XMR | Expectation or population mean of a random quantity | $E(x)$ | |
| x^A, x^{MS}, m_x | XMS | Average or sample mean of a random quantity | $1/n \sum x_i, i = 1 \dots n$ unbiased random estimate of the expectation with $x^{AE} = x^E$ $x^{VSE} = x^V / n$ | |
| x^{PD}, f_x | XPDP | Probability density of a random quantity | $d F_x / dx$ | |
| xy^{PD}, f_{xy} | XYPD | Joint probability density of two random quantities | $\partial^2 F_{xy} / (\partial x \partial y)$ | |
| x^{PF}, F_x | XPF | Probability function (distribution) of a random quantity | | 1 |
| xy^{PF}, F_{xy} | XYPF | Joint probability function (distribution) function of two random quantities | | 1 |
| x^V, x^{VR}, xt^{VR} | XVR, XXVR | Variance of a random quantity | $x^{2E} - x^E{}^2$ | |
| x^{VS}, xx^{VS} | XVS, XXVS | Sample variance of a random quantity | $1/(n-1) \sum (x_i - x^A)^2$ $i = 1 \dots n$ unbiased random estimate of the variance $x^{VSE} = x^V$ | |
| xy^V, xy^{VR} | XYVR | Variance of two random quantities | $x y^E - x^E y^E$ | |
| ζ | | Outcome of a random "experiment" | | |

1.1.4.2 Stochastic Processes

| | | | | |
|-------------------------|--------|---|---|--|
| g^{MR} | GMR | Mean of a function of a random quantity | $M(g(t)) = \lim(1/T \int g(t)dt)$ $t = -T/2 \dots +T/2$ $T = -\infty \dots +\infty$ | |
| g^{MS} | GMS | Average or sample mean of a function of a random quantity | $A(g(t)) = 1/T \int g(t)dt$ $t = 0 \dots +T$ | |
| x, y | X, Y | Stationary stochastic process | $x(\zeta, t), y(\zeta, t)$ | |
| xx^C, xx^{CR}, C_{xx} | XXCR | Auto-covariance of a stationary stochastic process | $(x(t) - x^E)(x(t + \tau) - x^E)^E$ | |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------------------|-----------------|--|---|---------|
| xy^C, xy^{CR}, C_{xy} | XYCR | Cross-covariance of two stationary stochastic processes | $(x(t) - x^E)(y(t + \tau) - y^E)^E$ | |
| xx^R, xx^{RR}, R_{xx} | XXRR | Auto-correlation of a stationary stochastic process | $x(t)x(t + \tau)^E = R_{xx}(\tau)$ $R_{xx}(\tau) = R_{xx}(-\tau)$ if x is ergodic: $R_{xx}(\tau) = x(t)x(t + \tau)^{MR}$ $R_{xx}(\tau) = \int S_{xx}(\omega)\cos(\omega\tau)d\tau$ $\tau = 0 \dots \infty$ | |
| xy^R, R_{xy} | XYRR | Cross-correlation of two stationary stochastic processes | $x(t)y(t + \tau)^E = R_{xy}(\tau)$ $R_{yx}(\tau) = R_{xy}(-\tau)$ if x, y are ergodic: $R_{xy}(\tau) = x(t)y(t + \tau)^{MR}$ | |
| xx^S, S_{xx} | XXSR | Power spectrum or autospectral power density of a stochastic process | xx^{RRSR} | |
| xy^S, S_{xy} | XYSR | Cross-power spectrum of two stationary stochastic processes | xy^{RRSR} | |
| τ | TICV | Covariance or correlation time | | s |
| ζ | | Outcome of a random "experiment" | | |

1.1.4.3 Probability Operators (Superscripts)

| | | |
|----------|----|------------------------------|
| A, MS | MS | Average, sample mean |
| C, CR | CR | Population covariance |
| CS | CS | Sample covariance |
| D, DR | DR | Population deviation |
| DS | DS | Sample deviation |
| E, M, MR | MR | Expectation, population mean |
| PD | PD | Probability density |
| PF | PF | Probability function |
| S | SR | (Power) Spectrum |
| SS | SS | Sample spectrum |
| R, RR | RR | Population correlation |
| RS | RS | Sample correlation |
| V, VR | VR | Population variance |
| VS | VS | Sample variance |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
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1.1.5 Balances and System Related Concepts

| | | | | |
|-------|-----|--|------------------|---------|
| q | QQ | Quantity of the quality under consideration stored in a control volume | | Q^U |
| Q | | Quality under consideration | | Q^U/s |
| Q^C | QCF | Convective flux | | Q^U/s |
| Q^D | QDF | Diffusive flux | | Q^U/s |
| Q^F | QFL | Total flux across the surface of the control volume | Inward positive! | Q^U/s |
| Q^M | | Molecular diffusion | | Q^U/s |
| Q^P | QPN | Production of sources in the control volume | | Q^U/s |
| Q^S | QRT | Storage in the control volume, rate of change of the quantity stored | dq / dt | Q^U/s |
| Q^T | QDT | Turbulent diffusion | | Q^U/s |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
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1.2 Solid Body Mechanics

1.2.1 Inertial and Hydrodynamic Properties

1.2.1.1 Basic Quantities

| | | | | |
|--|--|--|---|-------------------|
| A_{ij} | AM(I,J) | Added mass coefficient in i th mode due to j th motion | | |
| B_{ij} | DA(I,J) | Damping coefficient in i th mode due to j th motion | | |
| C_{ij} | RF(I,J) | Restoring force coefficient in i th mode due to j th motion | | |
| D_{uv}^h | DH(U,V) | Generalized hydrodynamic damping | $\partial F_u^h / \partial V_v$ | |
| F_u^h | FH(U) | Generalized hydrodynamic force | | |
| I_{uv}^h | IH(U,V) | Generalized hydrodynamic inertia | $\partial F_u^h / \partial \dot{V}_v$ | |
| I_L | IL | Longitudinal second moment of water-plane area | About transverse axis through centre of floatation | m ⁴ |
| I_T | IT | Transverse second moment of water-plane area | About longitudinal axis through centre of floatation | m ⁴ |
| $I_y, I_{yy}, m_{22}^2, m_{55}$ | IY, IYY, M2(2,2), MA(5,5) | Pitch moment of inertia around the principal axis y | | kg m ² |
| $I_z, I_{zz}, m_{33}^2, m_{66}$ | IZ, IZZ, M2(3,3), MA(6,6) | Yaw moment of inertia around the principal axis z | | kg m ² |
| $I_{xy}, I_{12}, I_{yz}, I_{23}, I_{zx}, I_{31}$ | IXY, I2(1,2), IYZ, I2(2,3), IZX, I2(3,1) | Real products of inertia in case of non-principal axes | | kg m ² |
| k_x, k_{xx}, k | RDGX | Roll radius of gyration around the principal axis x | $(I_{xx}/m)^{1/2}$ | m |
| k_y, k_{yy} | RDGY | Pitch radius of gyration around the principal axis y | $(I_{yy}/m)^{1/2}$ | m |
| k_z, k_{zz} | RDGZ | Yaw radius of gyration around the principal axis z | $(I_{zz}/m)^{1/2}$ | m |
| m | MA | mass | | kg |
| m_{ij}^0, m_{ij} | M0(I,J), MA(I,J) | Zero-th moments of mass, i.e. inertia distribution, mass tensor | $m_{ij} = m \delta_{ij}$ | kg |
| m_{ij}^1 | M1(I,J) | First moments of mass, i.e. inertia distribution | Alias static moments of mass | kg m |
| m_{ij}^2, I_{ij} | M2(I,J), IN(I,J) | Second moments of mass, i.e. inertia distribution | Alias mass moments of inertia | kg m ² |
| M_{uv} | MA(U,V) | Generalized mass, i. e. generalized inertia tensor of a (rigid) body referred to a body fixed co-ordinate system | $M_{ij} = M_{ij}^0$ $M_{i, 3+j} = M_{ij}^{1T}$ $M_{3+i, j} = M_{ij}^1$ $M_{3+i, 3+j} = M_{ij}^2$ | |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
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1.2.2 Loads

1.2.2.1 External Loads

| | | | | |
|-----------------------|----------------------|---|---|------------------|
| F_u | F(U) | Force, generalized, load, in body coordinates | $M_u^F = M_u^M$ $F_i = F_i^0$ $F_{3+i} = F_i^1$ | N |
| g_u | G(U) | Gravity field strength, generalized, in body coordinates | $g_i = g_i^1$ $g_{3+i} = 0$ | m/s ² |
| g_i | G1(I) | Gravity field strength, in body coordinates! | | m/s ² |
| K, M_x, F_1^1, F_4 | K, M(1), F1(1), F(4) | Moment around body axis x | | Nm |
| M, M_y, F_2^1, F_5 | M, M(2), F1(2), F(5) | Moment around body axis y | | Nm |
| N, M_z, FN_3^1, F_6 | N, M(3), F1(3), F(6) | Moment around body axis z | | Nm |
| X, F_x, F_1^0, F_1 | X, FX, F0(1), F(1) | Force in direction of body axis x | | Nm |
| Y, F_y, F_2^0, F_2 | Y, FY, F0(2), F(2) | Force in direction of body axis y | | Nm |
| Z, F_z, F_3^0, F_3 | Z, FZ, F0(3), F(3) | Force in direction of body axis z | | Nm |
| G_u | G(U) | Gravity or weight force, generalized, in body co-ordinates! | $G_u = m_{uv} g_v$ | N |
| $G^0 i, G_i$ | G0(I) | Gravity or weight force in body coordinates! | $G_i = G_i^0 = m_{ij}^0 g_j$ $= m g_i$ | N |
| G_i^1 | G1(I) | Gravity or weight moment in body coordinates! | $G_{3+i} = G_i^1 = \varepsilon_{ikj} x_k G_j^0$ $= m_{ij}^1 g_j$ | Nm |
| q | UNQ | Load per unit length | | N/m |
| w | WPUL | Weight per unit length | dW / dx_l | N/m |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

1.2.2.2 Sectional Loads

| | | | | |
|---------|--------------|--|--|---------|
| F^S_u | FS(U) | Force or load acting at a given planar cross-section of the body, generalized, in section coordinates! | $F^S_i = F^{S0}_i$ $F^{S_{3+i}} = F^{S1}_i = M^B_i$ | N Nm |
| F^S_i | FS(I) | Shearing force | F^{S0}_2, F^{S0}_3 | N |
| F^T | FT, FS(1) | Tensioning or normal force | F^{S0}_1 | N |
| M^B_i | MB(I) | Bending moment | F^{S1}_2, F^{S1}_3 | Nm |
| M^T | MT, MB(1) | Twisting or torsional moment | F^{S1}_1 | Nm |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
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1.2.3 Rigid Body Motions

1.2.3.1 Motions

| | | | | |
|-------------------------------------|---------------------|--|------------------------------------|--------------------|
| p, ω_x, v^0_1, v_4 | P, OMX, V0(1), V(4) | Rotational velocity around body axis x | | rad/s |
| q, ω_y, v^0_2, v_5 | Q, OMY, V0(2), V(5) | Rotational velocity around body axis y | | rad/s |
| r, ω_z, v^0_3, v_6 | R, OMZ, V0(3), V(6) | Rotational velocity around body axis z | | rad/s |
| u, v_x, v^1_1, v_1 | U, VX, V1(1), V(1) | Translatory velocity in the direction of body axis x | | m/s |
| v, v_y, v^1_2, v_2 | V, VY, V1(2), V(2) | Translatory velocity in the direction of body axis y | | m/s |
| w, v_z, v^1_3, v_3 | W, VZ, V1(3), V(3) | Translatory velocity in the direction of body axis z | | m/s |
| v_u | V(U) | Components of generalized velocity or motion relative to body axes | $v_i = v^1_i$ $v_{3+i} = v^0_i$ | m/s rad/s |
| \dot{p} \dot{q} \dot{r} | PR QR RR | Rates of change of components of rotational velocity relative to body axes | | rad/s ² |
| \dot{u} \dot{v} \dot{w} | UR VR WR | Rates of change of components of linear velocity relative to body axes | | m/s ² |
| α | AA | Angular acceleration | $d\omega/dt$ | rad/s ² |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

1.2.3.2 Attitudes

| | | | | |
|-----------|--------------------|---------------------------------|---|-----|
| α | AT ALFA | Angle of attack | The angle of the longitudinal body axis from the projection into the principal plane of symmetry of the velocity of the origin of the body axes relative to the fluid, positive in the positive sense of rotation about the y -axis | rad |
| β | DR BET | Angle of drift or side-slip | The angle to the principal plane of symmetry from the velocity vector of the origin of the body axes relative to the fluid, positive in the positive sense of rotation about the z -axis | rad |
| γ | RO GAMR | Projected angle of roll or heel | The angular displacement about the x_0 axis of the principal plane of symmetry from the vertical, positive in the positive sense of rotation about the x_0 axis | rad |
| φ | X(4) RO PHIR | Angle of roll, heel or list | Positive in the positive sense of rotation about the x -axis | rad |
| θ | X(5) TR TETP | Angle of pitch or trim | Positive in the positive sense of rotation about the y -axis | rad |
| ψ | X(6) YA PSIY | Angle of yaw, heading or course | Positive in the positive sense of rotation about the z -axis | rad |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
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1.3 Fluid Mechanics**1.3.1 Flow Parameters****1.3.1.1 Fluid Properties**

| | | | | |
|----------|---------|-----------------------|---------------------------------|--------------------------------|
| c | CS | Velocity of sound | $(E / \rho)^{1/2}$ | m/s |
| E | EL | Modulus of elasticity | | Pa |
| w | WD | Weight density | ρg (See 1.1.1) | |
| κ | CK | Kinematic capillarity | σ / ρ | m ³ /s ² |
| μ | VI | Viscosity | | kg/ms |
| ν | VK | Kinematic viscosity | μ / ρ | m ² /s |
| ρ | DN, RHO | Mass density | | kg/m ³ |
| σ | CA | Capillarity | Surface tension per unit length | kg/s ² |

1.3.1.2 Flow parameters

| | | | | |
|------------|------|------------------------------------|---|---|
| Bo | BN | Boussinesq number | $V / (g R_H)^{1/2}$ | 1 |
| Ca | CN | Cauchy number | $V / (E / \rho)^{1/2}$ | 1 |
| Fr | FN | Froude number | $V / (g L)^{1/2}$ | 1 |
| Fr_h | FH | Froude depth number | $V / (g h)^{1/2}$ | 1 |
| Fr_V | FV | Froude displacement number | $V / (g \nabla^{1/3})^{1/2}$ | 1 |
| Ma | MN | Mach number | V / c | 1 |
| Re | RN | Reynolds number | $V L / \nu$ | 1 |
| $Re_{0.7}$ | RN07 | Propeller Reynolds number at 0.7 R | $Re_{0.7} = \frac{c_{0.7} \sqrt{V_A^2 + (0.7 \pi n D)^2}}{\nu}$ | 1 |
| St | SN | Strouhal number | $f L / V$ | 1 |
| Th | TN | Thoma number, Cavitation number | $(p_A - p_v) / q$ | 1 |
| We | WN | Weber number | $V^2 L / \kappa$ | 1 |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

1.3.1.3 Boundary conditions

| | | | | |
|-------|----|-------------------------------|--|---|
| k | HK | Roughness height or magnitude | Roughness height, usually in terms of some average | m |
| k_s | SK | Sand roughness | Mean diameter of the equivalent sand grains covering a surface | m |
| R_H | RH | Hydraulic radius | Area of section divided by wetted perimeter | m |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
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1.3.2 Flow Fields

1.3.2.1 Velocities etc.

| | | | | |
|---|----------------------------|---|--|-------------------|
| e | ED | Density of total flow energy | $\rho V^2 / 2 + p + \rho g h$ | Pa |
| f_i | FS(I) | Mass specific force | Strength of force fields, usually only gravity field g_i | m/s ² |
| h | HS | Static pressure head | Δz_0 , z ₀ -axis positive vertical up! | m |
| H | HT | Total head | $e / w = h + p/w + q/w$ | m |
| p | PR, ES | Pressure, density of static flow energy | | Pa |
| p_0 | P0 | Ambient pressure in undisturbed flow | | Pa |
| q | PD, EK | Dynamic pressure, density of kinetic flow energy, | $\rho V^2 / 2$ | Pa |
| Q | QF, QFLOW | Rate of flow | Volume passing across a control surface in time unit | m ³ /s |
| S_H | THL | Total head loss | | m |
| s_{ij}^R | SR(I,J) | Turbulent or Reynolds stress | $\rho v_i v_j^{CR}$ | Pa |
| s_{ij} | ST(I,J) | Total stress tensor | Density of total diffusive momentum flux due to molecular and turbulent exchange | Pa |
| s_{ij}^V | SV(I,J) | Viscous stress | | Pa |
| u, v_x, v_1 v, v_y, v_2 w, v_z, v_3 | VX, V1 VY, V2 VZ, V3 | Velocity component in direction of x, y, z axes | | m/s |
| v_i | V(I) | Velocity | | m/s |
| V | VA | Velocity | $V = v_i v_i^{1/2}$ | m/s |
| V_0 | V0 | Velocity of undisturbed flow | | m/s |
| τ_w | TAUW | Wall shear stress | $\mu (\partial U / \partial y)_{y=0}$ | Pa |

1.3.2.2 Circulation etc.

| | | | | |
|------------|----|------------------------|--|-------------------|
| Γ^n | CN | Normalized circulation | $\Gamma / (\pi D V)$ π is frequently omitted | 1 |
| I | ID | Induction factor | Ratio between velocities induced by helicoidal and by straight line vortices | 1 |
| Γ | VD | Vortex density | Strength per length or per area of vortex distribution | m/s |
| Γ | CC | Circulation | $\oint V ds$ along a closed line | m ² /s |
| Φ | PO | Potential function | | m ² /s |
| Ψ | SF | Stream function | $\psi = \text{const}$ is the equation of a stream surface | m ³ /s |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
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1.3.3 Lifting Surfaces

1.3.3.1 Geometry

| | | | | |
|----------------|-------|--|-----------------|-------|
| A | AP | Projected area | $b c_M$ | m^2 |
| b | SP | Wing or foil span | | m |
| b_F | BSPF | Flap span | | m |
| c_M | CHME | Mean chord length | A / b | m |
| c_T | CHTP | Tip chord length | | m |
| c_r | CHRT | Root chord length | | m |
| f_L | FML | Camber of lower side (general) | | m |
| f_U | FMU | Camber of upper side | | m |
| γ | ANSW | Sweep angle | | rad |
| δ_s | ANSL | Slat deflection angle | | rad |
| δ | DELTT | Thickness ratio of foil section (general) | t / c | 1 |
| δ_B | DELTB | Thickness ratio of trailing edge of struts | t_B / c_s | 1 |
| δ_F | DELTF | Camber ratio of mean line (general) | f / c | 1 |
| δ_{FL} | DLTFL | Angle of flap deflection | | rad |
| δ_L | DELTL | Camber ratio of lower side of foil | f_L / c | 1 |
| δ_S | DELTS | Thickness ratio of strut | t_S / c_S | 1 |
| δ_{STH} | DELTT | Theoretical thickness ratio of section | t_S / c_{STH} | 1 |
| δ_U | DELTU | Camber ratio of upper side | f_U / c | 1 |
| λ | TA | Taper ratio | c_t / c_r | 1 |
| A | AS | Aspect ratio | b^2 / A | 1 |

1.3.3.2 Flow angles etc

| | | | | |
|----------------|------------|--|--|-----|
| V_I | VI | Induced velocity | | m/s |
| V_T | VT | Resultant velocity of flow approaching a hydrofoil | Taking vortex induced velocities into account | m/s |
| α | AA, ALFA | Angle of attack or incidence | Angle between the direction of undisturbed relative flow and the chord line | rad |
| α_{EFF} | AAEF, ALFE | Effective angle of attack or incidence | The angle of attack relative to the chord line including the effect of induced velocities | rad |
| α_G | AAGE, ALFG | Geometric angle of attack or incidence | The angle of attack relative to the chord line neglecting the effect of induced velocities | rad |
| α_H | AAHY, ALFI | Hydrodynamic angle of attack | In relation to the position at zero lift | rad |
| α_I | AAID, ALFS | Ideal angle of attack | For thin airfoil or hydrofoil, angle of attack for which the streamlines are tangent to the mean line at the leading edge. This condition is usually referred to as "shock-free" entry or "smooth" | rad |
| α_0 | AAZL, ALF0 | Angle of zero lift | Angle of attack or incidence at zero lift | rad |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

1.3.3.3 Forces

| | | | | |
|-----------|-------|--|--|---|
| D_F | DRF | Foil drag | Force in the direction of motion of an immersed foil | N |
| D_I | DRIND | Induced drag | For finite span foil, the component of lift in the direction of motion | N |
| D_{INT} | DRINT | Interference drag | Due to mutual interaction of the boundary layers of intersecting foil | N |
| D_P | DRSE | Section or profile drag at zero lift | Streamline drag | N |
| L_F | LF | Lift force on foil | $C_L A_{FT} q$ | N |
| L_0 | LF0 | Lift force for angle of attack of zero | $C_{L0} A_{FT} q$ | N |

1.3.3.4 Sectional coefficients

| | | | | |
|---------------|-------|--|-------|---|
| C_D | CDSE | Section drag coefficient | | 1 |
| C_{DI} | CDSI | Section induced drag coefficient | | 1 |
| C_L | CLSE | Section lift coefficient | | 1 |
| C_{L0} | CLSE0 | Section lift coefficient for angle of attack of zero | | 1 |
| C_M | CMSE | Section moment coefficient | | 1 |
| ε | EPSLD | Lift-Drag ratio | L/D | 1 |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

1.3.4 Boundary Layers

1.3.4.1 Two-dimensional Boundary Layers

| | | | | |
|-------------------------|--------|--|---|-------------------|
| C_f | CFL | Skin friction coefficient | $\tau / (\rho U_e^2 / 2)$ | 1 |
| F | CQF | Entrainment factor | $1 / (U_e dQ / dx)$ | 1 |
| H | HBL | Boundary layer shape parameter | δ^* / Θ | 1 |
| H_E | HQF | Entrainment shape parameter | $(\delta - \delta^*) / \Theta$ | 1 |
| p | PR | Static pressure | | Pa |
| P | PT | Total pressure | | Pa |
| Q | QF | Entrainment | $\int_a^b U dy$ | m ² /s |
| Re_{δ^*} | RDELS | Reynolds number based on displacement thickness | $U_\infty \delta^* / \nu$ or $U_e \delta^* / \nu$ | 1 |
| Re_θ | RTHETA | Reynolds number based on momentum thickness | $U_\infty \Theta / \nu$ or $U_e \Theta / \nu$ | 1 |
| u | UFL | Velocity fluctuations in boundary layer | | m/s |
| u^s | UFLS | Root mean square value of velocity fluctuations | | m/s |
| u^+ | UPLUS | Non-dimensional distance from surface | U / u_τ | 1 |
| u_τ | UTAU | Shear (friction) velocity | $(\tau / \rho)^{1/2}$ | m/s |
| U_m | UMR | Time mean of velocity in boundary layer | | m/s |
| U_i | UIN | Instantaneous velocity | | m/s |
| U_∞ | UFS | Free-stream velocity far from the surface | | m/s |
| U_e | UE | Velocity at the edge of the boundary layer at $y=\delta_{995}$ | | m/s |
| ΔU | UDEF | Velocity defect in boundary layer | $(U_e - U) / u_\tau$ | 1 |
| y^+ | YPLUS | Non-dimensional distance from the wall | $y u_\tau / \nu$ | 1 |
| β | BETE | Equilibrium parameter | $\delta^* / (\tau_w dp / dx)$ | 1 |
| δ_{995} | DEL | Thickness of a boundary layer at $U=0.995U_e$ | | m |
| δ^*, δ_1 | DELS | Displacement thickness of boundary layer | $\int (U_e - U) / U_e dy$ | m |
| K | K | von Karman constant | 0.41 | 1 |
| Λ | PRGR | Pressure gradient parameter | $\delta_{995} / (\nu dU_e / dx)$ | 1 |
| θ^*, δ^{**} | ENTH | Energy thickness | $\int (U / U_e) (1 - U^2 / U_e^2) dy$ | m |
| Θ | THETA | Momentum thickness | $\int (U / U_e) (1 - U / U_e) dy$ | m |
| τ_w | TAUW | Local skin friction | $\mu (\partial U / \partial y)_{y=0}$ | Pa |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

1.3.5 Cavitation

1.3.5.1 Flow parameters

| | | | | |
|------------|------|---------------------------------|---|-----|
| a_s | GR | Gas content ratio | α / a_s | 1 |
| α | GC | Gas content | Actual amount of solved and un-dissolved gas in a liquid | ppm |
| a_s | GS | Gas content of saturated liquid | Maximum amount of gas solved in a liquid at a given temperature | ppm |
| σ | CNPC | Cavitation number | $(p_A - p_c) / q$ | 1 |
| σ_i | CNPI | Inception cavitation number | | 1 |
| σ_v | CNPV | Vapour cavitation number | $(p_A - p_v) / q$ | 1 |

1.3.5.2 Flow fields

| | | | | |
|------------|------|----------------------------|---|----------------|
| D_C | DC | Cavity drag | | N |
| l_c | LC | Cavity length | Stream wise dimension of a fully-developed cavitating region | m |
| p_A | PA | Ambient pressure | | Pa |
| p_{AC} | PACO | Collapse pressure | Absolute ambient pressure at which cavities collapse | Pa |
| p_{AI} | PAIC | Critical pressure | Absolute ambient pressure at which cavitation inception takes place | Pa |
| p_c | PC | Cavity pressure | Pressure within a steady or quasi-steady cavity | Pa |
| p_{CI} | PCIN | Initial cavity pressure | Pressure, may be negative, i.e. tensile strength, necessary to create a cavity | Pa |
| p_v | PV | Vapour pressure of water | At a given temperature! | Pa |
| U_i | UNIN | Critical velocity | Free stream velocity at which cavitation inception takes place | m/s |
| V_L | VOLS | Volume loss | W_L / w | m ³ |
| W_L | WTLS | Weight loss | Weight of material eroded from a specimen during a specified time | N/s |
| δ_c | HC | Cavity height or thickness | Maximum height of a fully-developed cavity, normal to the surface and the stream-wise direction of the cavity | m |

1.3.5.3 Pumps

| | | | | |
|--------------|------|--------------------------------------|-------------------------|---|
| H_N | HTNT | Net useful head of turbo-engines | | m |
| H_U | HTUS | Total head upstream of turbo-engines | | m |
| Th, σ | TN | Thoma number | $(H_U - p_v / w) / H_N$ | 1 |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

1.4 Environmental Mechanics

1.4.1 Waves

This section is related to Sections 3.1.2 Time and Frequency Domain Quantities and 3.1.3 Random Quantities and Stochastic Processes.

1.4.1.1 Periodic waves

| | | | | |
|---------------------------|---------|---|---|-------|
| c_w | VP | Wave phase velocity or celerity | $L_w / T_w = \sqrt{gL_w / 2\pi}$ in deep water | m/s |
| c_{wi} | VP(I) | Wave phase velocity of harmonic components of a periodic wave | const = c_w for periodic waves in deep water | m/s |
| c_G | VG | Wave group velocity or celerity | The average rate of advance of the energy in a finite train of gravity waves | m/s |
| f_w | FW | Basic wave frequency | $1 / T_w$ | Hz |
| f_{wi} | FW(I) | Frequencies of harmonic components of a periodic wave | $i f_w$ | Hz |
| H_w | HW | Wave height | The vertical distance from wave crest to wave trough, or twice the wave amplitude of a harmonic wave. $\eta_C - \eta_T$ | m |
| k, κ | WN | Wave number | $2\pi / L_w = \omega^2 / g$ | 1/m |
| L_w, λ_w | LW | Wave length | The horizontal distance between adjacent wave crests in the direction of advance | m |
| T_w | TW | Basic wave period | Time between the passage of two successive wave crests past a fixed point. $1 / f_w$ | s |
| μ | WD | Wave direction | The angle between the direction of a component wave and the x_0 axis | rad |
| η | EW | Instantaneous wave elevation at a given location | z-axis positive vertical up, zero at mean water level; | m |
| η_i^a | EWAM(I) | Amplitudes of harmonic components of a periodic wave | η^{FSa} | m |
| η_i^p, ε_i | EWPH(I) | Phases of harmonic components of a periodic wave | η^{FSp} | rad |
| η_C | EC | Wave crest elevation | | m |
| η_T | ET | Wave trough depression | Negative values! | m |
| ζ | DW | Instantaneous wave depression | z-axis positive vertical down, zero at mean water level | m |
| ζ_A | WAMP | Wave amplitude | Radius of orbital motion of a surface wave particle | m |
| ω_w, σ | FC | Circular wave frequency | $2\pi f_w = 2\pi / T_w$ | rad/s |

1.4.1.2 Irregular waves

| | | | | |
|-------|----|-----------------------------------|--|---|
| H_d | HD | Wave height by zero down-crossing | The vertical distance between a successive crest and trough. | m |
| H_u | HU | Wave height by zero up-crossing | The vertical distance between a successive trough and crest | m |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|--|--|---------|
| $H_{W1/3}$ | H13D | Significant wave height | Average of the highest one third zero down-crossing wave heights | m |
| $T_{1/3d}$ | T13D | Significant wave period | By downcrossing analysis | s |
| $T_{1/3u}$ | T13U | Significant wave period | By upcrossing analysis | s |
| T_d | TD | Wave periods by zero down-crossing | Time elapsing between two successive downward crossings of zero in a record | s |
| T_u | TU | Wave periods by zero up-crossing | Time elapsing between two successive upward crossings of zero in a record | s |
| η_c | EC | Maximum of elevations of wave crests in a record | | m |
| η_T | ET | Elevations of wave troughs in a record | Negative values! | m |
| λ_d | LD | Wave length by zero down-crossing | The horizontal distance between adjacent down crossing in the direction of advance | m |
| λ_u | LU | Wave length by zero up-crossing | The horizontal distance between adjacent up crossing in the direction of advance | m |

1.4.1.3 Time Domain Analysis

| | | | | |
|------------|------|--|--|---|
| H_{WV} | HWV | Wave height estimated from visual observation | | m |
| $H_{1/3d}$ | H13D | Zero down-crossing significant wave height | Average of the highest one third zero down-crossing wave heights | m |
| $H_{1/3u}$ | H13U | Zero up-crossing significant wave height | Average of the highest one third zero up-crossing wave heights | m |
| H_σ | HWDS | Estimate of significant wave height from sample deviation of wave elevation record | | m |
| L_{WV} | LWV | Wave length estimated by visual observation | Measured in the direction of wave propagation | m |
| T_R | TRT | Return period | The average interval in years between times that a given design wave is exceeded | |
| T_R | TR | Duration of record | $1/f_R$ | s |
| T_S | TS | Sample interval | $1/f_S$, time between two successive samples | s |
| T_{WV} | TWV | Wave period estimated from visual observation | | s |

1.4.1.4 Frequency Domain Analysis

| | | | | |
|----------|------|---|--|----|
| b | B | Bandwidth of spectral resolution | Sampling frequency divided by the number of transform points | Hz |
| C_r | CRA | Average reflection coefficient | | 1 |
| $C_r(f)$ | CRF | Reflection coefficient amplitude function | | 1 |
| f_P | FRPK | Spectral peak in frequency | Frequency at which the spectrum has its maximum | Hz |
| f_R | FRRC | Frequency resolution | $1/T_R$ | Hz |
| f_S | FRSA | Sample frequency | $1/T_S$ | Hz |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-----------------------------------|-----------------|--|---------------------------|-----------|
| H_{mo} | HMO | Significant wave height based on zeroth moment for narrow banded spectrum | $4 (m_0)^{1/2}$ | m |
| H_σ | HWDS | Estimate of significant wave height from sample deviation of wave elevation record | | m |
| m_n | MN | n-th moment of wave power spectral density | $\int f^n S(f) df$ | m^2/s^n |
| $S_i(f)$, $S_i(\omega)$ | EISF, EISC | Incident wave power spectral density | | m^2/Hz |
| $S_r(f)$, $S_r(\omega)$ | ERSF, ERSC | Reflected wave power spectral density | | m^2/Hz |
| $S_\eta(f)$, $S_\eta(\omega)$ | EWSF, EWSC | Wave power spectral density | | m^2/Hz |
| T_P | TP | Period with maximum energy | $2\pi f_P$ | s |
| T_{01} | T1 | Average period from zeroth and first moment | m_0/m_1 | s |
| T_{02} | T2 | Average period from zeroth and second moment | $(m_0/m_2)^{1/2}$ | s |

1.4.1.5 Directional Waves

| | | | | |
|---|------------------------|----------------------------------|--|--------------|
| $D_x(f, \theta)$, $D_x(\omega, \mu)$, σ_θ | DIRSF SIGMAOX | Directional spreading function | $S(f, \theta) = S(f) D_x(f, \theta)$ where $\int_0^{2\pi} D_x(f, \theta) d\theta = 1$ | rad |
| f | FR | Frequency | $2\pi\omega = 1/T$ | Hz |
| $S_\zeta(\omega, \mu)$ $S_\theta(\omega, \mu)$ etc. | S2ZET S2TET etc. | Two dimensional spectral density | | 1 |
| $S_p(f, \theta)$ $S_\zeta(\omega, \mu)$ | STHETA | Directional spectral density | | $m^2/Hz/rad$ |
| θ, μ | CWD | Component wave direction | | rad |
| θ_m | MWD THETAMOX | Mean or dominant wave direction | | rad |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

1.4.2 Wind

1.4.2.1 Basic Quantities

| | | | | |
|---------------|--------|--|--|-----|
| C_{10} | C10M | Surface drag coefficient | $(0.08 + 0.065U_{10})10^{-3}$ | |
| F | FETCH | Fetch length | Distance over water the wind blows | m |
| t_d | DURATN | Wind duration | | s |
| T_r | TRT | Return period | The average interval in years between times that a given wind speed is exceeded | |
| u_z, u_{zi} | UFLUCT | Turbulent wind fluctuations | | m/s |
| U_A, u^* | USHEAR | Wind shear velocity | $C_{10}^{1/2} U_{10}$ or $0.71U_{10}^{1.23}$ | m/s |
| U_{10} | U10M | Reference mean wind speed at elevation 10 meters above sea surface | $U_{10} = (10/z)^{1/7} U_z^A$ | m/s |
| U_z^A | UZA | Average wind speed at elevation z above the sea surface | $(U_z + u_{zi})^A$ $U_z^A = (z/10)^{1/7} U_{10}$ or $U_z^A = U_{10} + U_A \ln(z/10)$ | m/s |
| V_{WR} | VWREL | Apparent wind velocity | see section 1.4.1 | m/s |
| V_{WT} | VWABS | True wind velocity | see section 1.4.1 | m/s |
| X_F | FDIM | Dimensionless Fetch | gF/U_{10}^2 | |
| z | ZSURF | Height above the sea surface in meters | | m |
| β_{WA} | BETWA | Apparent wind angle (relative to vessel course) | see section 2.6 | rad |
| β_{WT} | BETWT | True wind angle (relative to vessel course) | see section 2.6 | rad |
| θ_W | TETWI | Wind direction | | rad |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

1.4.3 Ice Mechanics

1.4.3.1 Basic Quantities

| | | | | |
|-----------------------|---------|------------------------------|--|-------------------|
| E_I | MEI | Modulus of elasticity of ice | | Pa |
| S_I | SAIC | Salinity of ice | Weight of salt per unit weight of ice | 1 |
| S_W | SAWA | Salinity of water | Weight of dissolved salt per unit weight of saline water | 1 |
| t_A | TEAI | Temperature of air | | °C |
| t_I | TEIC | Local temperature of ice | | °C |
| t_W | TEWA | Temperature of water | | °C |
| δ_I | ELIC | Deflection of ice sheet | Vertical elevation of ice surface | m |
| ε_I | STIC | Ice strain | Elongation per unit length | 1 |
| $\dot{\varepsilon}_I$ | STR TIC | Ice strain rate | $\partial \varepsilon / \partial t$ | 1/s |
| μ_I | POIIC | Poisson's ratio of ice | | 1 |
| v_A | POAI | Relative volume of air | Volume of gas pores per unit volume of ice | 1 |
| v_B | POBR | Relative volume of brine | Volume of liquid phase per unit volume of ice | 1 |
| v_0 | POIC | Total porosity of ice | $v_0 = v_A + v_B$ | 1 |
| ρ_I | DNIC | Mass density of ice | Mass of ice per unit volume | kg/m ³ |
| ρ_{SN} | DNSN | Mass density of snow | Mass of snow per unit volume | kg/m ³ |
| ρ_W | DNWA | Mass density of water | | kg/m ³ |
| ρ_A | DNWI | Density difference | $\rho_A = \rho_W - \rho_I$ | kg/m ³ |
| σ_{CI} | SCIC | Compressive strength of ice | | Pa |
| σ_{FI} | SFIC | Flexural strength of ice | | Pa |
| σ_{TI} | SNIC | Tensile strength of ice | | Pa |
| τ_{SI} | STIC | Shear strength of ice | | Pa |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

1.5 Noise**1.5.1 Underwater Noise**

| | | | | |
|-------|------|---|---|----|
| d | DIDR | Distance hydrophone to acoustic centre | | m |
| L_p | SPL | Sound pressure level | $L_p = 10 \log_{10} \left(\frac{\bar{p}_{rms}^2}{p_{ref}^2} \right) \text{dB}, p_{ref} = 1 \mu\text{Pa}$ | |
| L_s | SRNL | Underwater sound radiated noise level at a reference distance of 1m | $L_s = L_p + 20 \log_{10} \left[\frac{d}{d_{ref}} \right] \text{dB}, d_{ref} = 1 \text{ m}$ | |
| p | SPRE | Sound pressure | | Pa |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

2. SHIPS IN GENERAL

2.1 Basic Quantities

| | | | | |
|------------|--------------|--|--|-------------------|
| a, a^1 | AC, A1 | Linear or translatory acceleration | dv / dt | m/s ² |
| A | A, AR, AREA | Area in general | | m ² |
| B | B, BR | Breadth | | m |
| C, F^F_2 | FF(2) | Cross force | Force normal to lift and drag (forces) | N |
| C_c | CC | Cross force coefficient | $C_c = \frac{C}{qA}$ | 1 |
| D, F^F_1 | FF(1) | Resistance, Drag (force) | Force opposing translatory velocity, generally for a completely immersed body | N |
| d, D | D, DI | Diameter | | m |
| E | E, EN | Energy | | J |
| f | FR | Frequency | $1 / T$ | Hz |
| F, F^0 | F, F0 | Force | | N |
| g | G, GR | Acceleration of gravity | Weight force / mass, strength of the earth gravity field | m/s ² |
| h | DE | Depth | | m |
| H | H, HT | Height | | m |
| I | I, IN | Moment of inertia | Second order moment of a mass distribution | kg m ² |
| L | L, LE | Length | | m |
| L, F^F_3 | FF(3) | Lift (force) | Force perpendicular to translatory velocity | N |
| m | M, MA, MASS | Mass | | kg |
| M, F^1 | M1, F1 | Moment of forces | First order moment of a force distribution | Nm |
| M | MO | Momentum | | Ns |
| n, N | FR, N | Frequency or rate of revolution | Alias RPS (RPM in some propulsor applications) | Hz |
| P | P, PO | Power | | W |
| r, R | RD | Radius | | m |
| R, F^F_1 | R, RE, FF(1) | Resistance (force) | Force opposing translatory velocity | N |
| s | SP | Distance along path | | m |
| t | TI | Time | | s |
| t | TE | Temperature | | K |
| T | TC | Period | Duration of a cycle of a repeating or periodic, not necessarily harmonic process | s |
| U | U, UN | Undisturbed velocity of a fluid | | m/s |
| v, V^1 | V, V1 | Linear or translatory velocity of a body | ds / dt | m/s |
| V | VO | Volume | | m ³ |
| w | WD | Weight density, formerly specific weight | $dW / dV = \rho g$ | N/m ³ |
| W | WT | Weight (force), gravity force acting on a body | | N |
| γ | MR | Relative mass or weight, in English speaking countries called specific gravity | Mass density of a substance divided by mass density of distilled water at 4°C | 1 |
| η | EF, ETA | Efficiency | Ratio of powers | |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|--|---|-------------------|
| ρ | DN, RHO | Mass density | dm / dV | kg/m ³ |
| ρ_0 | RHO0 | water density for reference water temperature and salt content | | kg/m ³ |
| ρ_A | DNA, RHOA | Mass density of air | Mass of air per unit volume | kg/m ³ |
| τ | ST, TAU | Tangential stress | | Pa |
| λ | SC | Scale ratio | Ship dimension divided by corresponding model dimension | 1 |
| σ | SN, SIGS | Normal stress | | Pa |
| ω | FC, OMF | Circular frequency | $2 \pi f$ | 1/s |
| ω, V^0 | V0, OMN | Rotational velocity | $2 \pi n$ | rad/s |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

2.2 Geometry and Hydrostatics

2.2.1 Hull Geometry

2.2.1.1 Basic Quantities

| | | | | |
|----------|-------|---|--|----------------|
| A_{BL} | ABL | Area of bulbous bow in longitudinal plane | The area of the ram projected on the middle line plane forward of the fore perpendicular | m ² |
| A_{BT} | ABT | Area of transverse cross-section of a bulbous bow (full area port and star-board) | The cross sectional area at the fore perpendicular. Where the water lines are rounded so as to terminate on the forward perpendicular A_{BT} is measured by continuing the area curve forward to the perpendicular, ignoring the final rounding. | m ² |
| A_M | AM | Area of midship section | Midway between fore and aft perpendiculars | m ² |
| A_T | ATR | Area of transom (full area port and starboard) | Cross-sectional area of transom stern below the load waterline | m ² |
| A_V | AV | Area exposed to wind | Area of portion of ship above waterline projected normally to the direction of relative wind | m ² |
| A_W | AW | Area of water-plane | | m ² |
| A_{WA} | AWA | Area of water-plane aft of midship | | m ² |
| A_{WF} | AWF | Area of water-plane forward of midship | | m ² |
| A_X | AX | Area of maximum transverse section | | m ² |
| B | B | Beam or breadth, moulded, of ships hull | | m |
| B_M | BM | Breadth, moulded of midship section at design water line | | m |
| B_T | BTR | Breadth, moulded of transom at design water line | | m |
| B_{WL} | BWL | Maximum moulded breadth at design water line | | m |
| B_X | BX | Breadth, moulded of maximum section area at design water line | | m |
| d, T | T | Draught, moulded, of ship hull | | m |
| d_{KL} | KDROP | Design drop of the keel line | $T_{AD} - T_{FD}$ alias "keel drag" or "slope of keel" | m |
| D | DEP | Depth, moulded, of a ship hull | | m |
| f | FREB | Freeboard | From the freeboard markings to the freeboard deck, according to official rules | m |
| i_E | ANEN | Angle of entrance, half | Angle of waterline at the bow with reference to centre plane, neglecting local shape at stem | rad |
| i_R | ANRU | Angle of run, half | Angle of waterline at the stern with reference to the centre-plane, neglecting local shape of stern frame | rad |
| L | L | Length of ship | Reference length of ship (generally length between the perpendiculars) | m |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|----------------|-----------------|---|---|----------------|
| L_E | LEN | Length of entrance | From the forward perpendicular to the forward end of parallel middle body, or maximum section | m |
| L_{OA} | LOA | Length, overall | | m |
| L_{OS} | LOS | Length, overall submerged | | m |
| L_P | LP | Length of parallel middle body | Length of constant transverse section | m |
| L_{PP} | LPP | Length between perpendiculars | | m |
| L_R | LRU | Length of run | From section of maximum area or after end of parallel middle body to waterline termination or other designated point of the stern | m |
| L_{WL} | LWL | Length of waterline | | m |
| L_{FS} | LFS | Frame spacing | used for structures | m |
| L_{SS} | LSS | Station spacing | | m |
| S | S, AWS | Area of wetted surface | | m ² |
| t | TT | Taylor tangent of the area curve | The intercept of the tangent to the sectional area curve at the bow on the midship ordinate | 1 |
| T, d | T | Draught, moulded, of ship hull | | m |
| T_A, d_A | TA, TAP | Draught at aft perpendicular | | m |
| T_{AD} | TAD, TAPD | Design draught at aft perpendicular | | m |
| T_F, d_F | TF, TFP | Draught at forward perpendicular | | m |
| T_{FD} | TFD, TFPD | Design draught at forward perpendicular | | m |
| T_H | THUL | Draught of the hull | Maximum draught of the hull without keel or skeg | m |
| T_M, d_M | TM, TMS | Draught at midship | $(T_A + T_F) / 2$ for rigid bodies with straight keel | m |
| T_{MD} | TMD, TMSD | Design draught at midship | $(T_{AD} + T_{FD}) / 2$ for rigid bodies | m |
| T_T | TTR | Immersion of transom | Vertical depth of trailing edge of boat at keel below water surface level | m |
| ∇, V | DISPVOL | Displacement volume | $\Delta / (\rho g) = \nabla_{BH} + \nabla_{AP}$ | m ³ |
| ∇_{BH} | DISPVBH | Displacement volume of bare hull | $\Delta_{BH} / (\rho g)$ | m ³ |
| ∇_{APP} | DISPVAP | Displacement volume of appendages | $\Delta_{AP} / (\rho g)$ | m ³ |
| Δ | DISPF | Displacement force (buoyancy) | $g \rho \nabla$ | N |
| Δ_{BH} | DISPFBH | Displacement force (buoyancy) of bare hull | $g \rho \nabla_{BH}$ | N |
| Δ_{APP} | DISPFAP | Displacement force (buoyancy) of appendages | $g \rho \nabla_{AP}$ | N |
| Δ_m | DISPM | Displacement mass | $\rho \nabla$ | kg |
| λ | SC | Linear scale of ship model | $\lambda = L_S / L_M = B_S / B_M = T_S / T_M$ | 1 |

2.2.1.2 Derived Quantities

| | | | | |
|----------|-------|---|--------------------------------|---|
| B^C | CIRCB | R.E. Froude's breadth coefficient | $B / \nabla^{1/3}$ | 1 |
| C_B | CB | Block coefficient | $\nabla / (L B T)$ | 1 |
| C_{GM} | CGM | Dimensionless \overline{GM} coefficient | $\overline{GM} / \nabla^{1/3}$ | 1 |
| C_{GZ} | CGZ | Dimensionless \overline{GZ} coefficient | $\overline{GZ} / \nabla^{1/3}$ | 1 |
| C_{KG} | CKG | Dimensionless \overline{KG} coefficient | \overline{KG} / T | 1 |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|--|--|---------|
| C_{IL} | CWIL | Coefficient of inertia of water plane, longitudinal | $12 I_L / (B L^3)$ | 1 |
| C_{IT} | CWIT | Coefficient of inertia of water plane, transverse | $12 I_T / (B^3 L)$ | 1 |
| C_M | CMS | Midship section coefficient (mid-way between forward and aft perpendiculars) | $A_M / (B T)$ | 1 |
| C_P | CPL | Longitudinal prismatic coefficient | $\nabla / (A_X L)$ or $\nabla / (A_M L)$ | 1 |
| C_{PA} | CPA | Prismatic coefficient, after body | $\nabla_A / (A_X L / 2)$ or $\nabla_A / (A_M L / 2)$ | 1 |
| C_{PE} | CPE | Prismatic coefficient, entrance | $\nabla_E / (A_X L_E)$ or $\nabla_E / (A_M L_E)$ | 1 |
| C_{PF} | CPF | Prismatic coefficient fore body | $\nabla_F / (A_X L / 2)$ or $\nabla_F / (A_M L / 2)$ | 1 |
| C_{PR} | CPR | Prismatic coefficient, run | $\nabla_R / (A_X L_R)$ or $\nabla_R / (A_M L_R)$ | 1 |
| C_S | CS | Wetted surface coefficient | $S / (V L)^{1/2}$ | 1 |
| C_{VP} | CVP | Prismatic coefficient vertical | $\nabla / (A_W T)$ | 1 |
| C_{WA} | CWA | Water plane area coefficient, aft | $A_{WA} / (B L / 2)$ | 1 |
| C_{WF} | CWF | Water plane area coefficient, forward | $A_{WF} / (B L / 2)$ | 1 |
| C_{WP} | CW | Water plane area coefficient | $A_W / (L B)$ | 1 |
| C_X | CX | Maximum transverse section coefficient | $A_X / (B T)$, where B and T are measured at the position of maximum area | 1 |
| C_V | CVOL | Volumetric coefficient | ∇ / L^3 | 1 |
| f_{BL} | CABL | Area coefficient for bulbous bow | $A_{BL} / (L T)$ | 1 |
| f_{BT} | CABL | Taylor sectional area coefficient for bulbous bow | A_{BT} / A_X | 1 |
| f_T | ATR | Sectional area coefficient for transom stern | A_T / A_X | 1 |
| M^C | CIRCM | R.E. Froude's length coefficient, or length-displacement ratio | $L / \nabla^{1/3}$ | 1 |
| S^C | CIRCS | R.E. Froude's wetted surface area coefficient | $S / \nabla^{2/3}$ | 1 |
| T^C | CIRCT | R.E. Froude's draught coefficient | $T / \nabla^{1/3}$ | 1 |

2.2.1.3 Symbols for Attributes and Subscripts

| | | |
|-----|-----|---------------------|
| A | AB | After body |
| AP | AP | After perpendicular |
| APP | APP | Appendages |
| B | BH | Bare hull |
| | DW | Design waterline |
| E | EN | Entry |
| F | FB | Fore body |
| FP | FP | Fore perpendicular |
| FS | FS | Frame spacing |
| H | HE | Hull |
| | LR | Reference Line |
| LP | LP | Based on LPP |
| LW | LW | Based on LWL |
| M | MS | Midships |
| | PB | Parallel body |
| R | RU | Run |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|-----------------|------------------------------|-------------|
| SS | SS | Station spacing | | |
| W | WP | Water plane | | |
| S | WS | Wetted surface | | |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

2.2.2 Propulsor Geometry

2.2.2.1 Screw Propellers

| | | | | |
|------------------------|------|----------------------------------|--|----------------|
| A_D | AD | Developed blade area | Developed blade area of a screw propeller outside the boss or hub | m ² |
| A_E | AE | Expanded blade area | Expanded blade area of a screw propeller outside the boss or hub | m ² |
| A_0 | AO | Propeller Disc Area | $\pi D^2 / 4$ | m ² |
| A_P | AP | Projected blade area | Projected blade area of a screw propeller outside the boss or hub | m ² |
| a_D | ADR | Developed blade area ratio | A_D / A_0 | 1 |
| a_E | ADE | Expanded blade area ratio | A_E / A_0 | 1 |
| a_P | ADP | Projected blade area ratio | A_P / A_0 | 1 |
| c | LCH | Chord length | | m |
| $c_{0.7}$ | C07 | Chord length | Chord length at r/R=0.7 | m |
| c_{LE} | CHLE | Chord, leading part | The part of the Chord delimited by the Leading Edge and the intersection between the Generator Line and the pitch helix at the considered radius | m |
| c_M | CHME | Mean chord length | The expanded or developed area of a propeller blade divided by the span from the hub to the tip | m |
| c_s | CS | Skew displacement | The displacement between middle of chord and the blade reference line. Positive when middle chord is at the trailing side regarding the blade reference line | m |
| c_{TE} | CHTE | Chord, trailing part | The part of the Chord delimited by the Trailing Edge and the intersection between the Generator Line and the pitch helix at the considered radius | m |
| d_h | DH | Boss or hub diameter | $2 r_h$ | m |
| d_{ha} | DHA | Hub diameter, aft | Aft diameter of the hub, not considering any shoulder | m |
| d_{hf} | DHF | Hub diameter, fore | Fore diameter of the hub, not considering any shoulder | m |
| D | DP | Propeller diameter | | m |
| f | FBP | Camber of a foil section | | m |
| G_Z | GAP | Gap between the propeller blades | $2 \pi r \sin(\varphi) / z$ | m |
| h_0 | HO | Immersion | The depth of submergence of the propeller measured vertically from the propeller centre to the free surface | m |
| H_{TC} | HTC | Hull tip clearance | Distance between the propeller sweep circle and the hull | m |
| $i_G, R_k(\text{ISO})$ | RAKG | Rake | The displacement from the propeller plane to the generator line in the direction of the shaft axis. Aft displacement is positive rake. | m |
| i_s | RAKS | Rake, skew-induced | The axial displacement of a blade section which occurs when the propeller is skewed. Aft displacement is positive rake | m |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|--------------------------|-----------------|--|---|---------|
| i_T | RAKT | Rake, total | The axial displacement of the blade reference line from the propeller plane $i_G + i_S = c_S \sin \phi$ Positive direction is aft. | m |
| l_h | LH | Hub length | The length of the hub, including any fore and aft shoulder | m |
| l_{ha} | LHA | Hub length, aft | Length of the hub taken from the propeller plane to the aft end of the hub including aft shoulder | m |
| l_{hf} | LHF | Hub length, fore | Length of the hub taken from the propeller plane to the fore end of the hub including fore shoulder | m |
| N_P | NPR | Number of propellers | | 1 |
| p | PDR | Pitch ratio | P / D | 1 |
| P | PITCH | Propeller pitch in general | | m |
| r | LR | Blade section radius | | m |
| r_h | RH | Hub radius | | m |
| R | RDP | Propeller radius | | m |
| t | TM | Blade section thickness | | m |
| t_0 | TO | Thickness on axis of propeller blade | Thickness of propeller blade as extended down to propeller axis | m |
| x_B | XBDR | Boss to diameter ratio | d_h / D | |
| x_P | XP | Longitudinal propeller position | Distance of propeller centre forward of the after perpendicular | m |
| y_P | YP | Lateral propeller position | Transverse distance of wing propeller centre from middle line | m |
| Z, z | NPB | Number of propeller blades | | 1 |
| z_P | ZP | Vertical propeller position | Height of propeller centre above base line | m |
| ε, ψ^{bP} | PSIBP | Propeller axis angle measured to body fixed coordinates | Angle between reference line and propeller shaft axis | rad |
| θ_s | TETS | Skew angle | The angular displacement about the shaft axis of the reference point of any blade section relative to the generator line measured in the plane of rotation. It is positive when opposite to the direction of ahead rotation | rad |
| θ | RAKA | Angle of rake | | rad |
| θ_{EXT} | TEMX | Skew angle extent | The difference between maximum and minimum local skew angle | rad |
| ϕ | PHIP | Pitch angle of screw propeller | $\arctg (P / (2 \pi R))$ | 1 |
| ϕ_F | PHIF | Pitch angle of screw propeller measured to the face line | | 1 |
| ψ^{aP} | PSIAP | Propeller axis angle measured to space fixed coordinates | Angle between horizontal plane and propeller shaft axis | rad |
| τ_B | | Blade thickness ratio | t_0 / D | 1 |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

2.2.2.2 Ducts

| | | | | |
|------------|--------|-------------------------------|--|----------------|
| A_{DEN} | ADEN | Duct entry area | | m ² |
| A_{DEX} | ADEX | Duct exit area | | m ² |
| d_D | CLEARD | Propeller tip clearance | Clearance between propeller tip and inner surface of duct | m |
| f_D | FD | Camber of duct profile | | m |
| L_D | LD | Duct length | | m |
| L_{DEN} | LDEN | Duct entry part length | Axial distance between leading edge of duct and propeller plane | m |
| L_{DEX} | LDEX | Duct exit length | Axial distance between propeller plane and trailing edge of duct | m |
| t_D | TD | Thickness of duct profile | | m |
| α_D | AD | Duct profile-shaft axis angle | Angle between nose-tail line of duct profile and propeller shaft | rad |
| β_D | BD | Diffuser angle of duct | Angle between inner duct tail line and propeller shaft | rad |

2.2.2.3 Waterjets (see also section 1.3.5)

| | | | | |
|------------|--|---|----------------------|----------------|
| A_n, A_6 | | Nozzle discharge area | | m ² |
| A_s | | Cross sectional area at station s | | m ² |
| D | | Impeller diameter (maximum) | | m |
| D_n | | Nozzle discharge diameter | | m |
| H_{ij} | | Head between station i and j | | m |
| H_{JS} | | Jet System Head | | m |
| h_{1A} | | maximum height of cross sectional area of stream tube at station 1A | | m |
| K_H | | Head coefficient: | $\frac{gH}{n^2 D^5}$ | 1 |

2.2.2.4 Pods

| | | | | |
|------------|-------|--------------------------------------|--|----------------|
| A_{PB} | APB | Wetted Surface Area of Pod Main Body | | m ² |
| A_{PBF} | APBF | Wetted Surface Area of Bottom Fin | | m ² |
| A_{PS} | APS | Wetted Surface Area of Strut | | m ² |
| C_{BFTC} | CBFTC | Thickness Cord Ratio of Bottom Fin | | 1 |
| C_{STC} | CSTC | Thickness Cord Ratio of Strut | | 1 |
| D_{PB} | DPB | Maximum Diameter of Pod Body | | m |
| L_{PB} | LPB | Length of Pod Main Body | | m |
| L_{PBF} | LPBF | Length of Bottom Fin | Code length of bottom fin under pod main body | m |
| L_{PS} | LPS | Length of Upper Strut | Code length of strut between forward edge and aft edge | m |
| T_{PBS} | TPBS | Bottom Thickness of Strut | | m |

2.2.2.5 Operators and identifiers

| | | |
|---|----------------------------|---------------|
| a | absolute (space) reference | (superscript) |
| b | body axis reference | (superscript) |
| P | propeller shaft axis | (subscript) |
| D | Duct | (subscript) |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

2.2.3 Appendage Geometry

Related information may be found in Section 3.3.3 on Lifting Surfaces.

2.2.3.1 Basic Quantities

| | | | | |
|-----------------|--------|---|---|----------------|
| A_C | AC | Area under cut-up | | m ² |
| A_{FB} | AFB | Area of bow fins | | m ² |
| A_{FR} | AFR | Frontal area | Projected frontal area of an appendage | m ² |
| A_{RF} | AF | Projected flap area | | m ² |
| A_R | ARU | Lateral rudder area | Area of the rudder, including flap | m ² |
| A_{RX} | ARX | Lateral area of the fixed part of rudder | | m ² |
| A_{RP} | ARP | Lateral area of rudder in the propeller race | | m ² |
| A_{RT} | ART | Total lateral rudder area | $A_{RX} + A_{Rmov}$ | m ² |
| A_{FS} | AFS | Projected area of stern fins | | m ² |
| A_{SK} | ASK | Projected skeg area | | m ² |
| S_{WBK} | SWBK | Wetted surface area of bilge keels | | m ² |
| c | CH | Chord length of foil section | | m |
| c_M | CHME | Mean chord length | A_{RT}/S | m |
| c_R | CHRT | Chord length at the root | | m |
| c_T | CHTP | Chord length at the tip | | m |
| f | FM | Camber of an aerofoil or a hydrofoil | Maximum separation of median and nose-tail line | m |
| L_F | LF | Length of flap or wedge | Measured in direction parallel to keel | m |
| t | TMX | Maximum thickness of an aerofoil or a hydrofoil | Measured normal to mean line | m |
| α_{FB} | ANFB | Bow fin angle | | rad |
| α_{FS} | ANFS | Stern fin angle | | rad |
| δ_F | DELFS | Flap angle (general) | Angle between the planing surface of a flap and the bottom before the leading edge | rad |
| δ_W | DELWG | Wedge angle | Angle between the planing surface of a wedge and the bottom before the leading edge | rad |
| δ_{FR} | ANFR | Flanking rudder angle | | rad |
| δ_{FRin} | ANFRIN | Assembly angle of flanking rudders | Initial angle set up during the assembly as zero angle of flanking rudders | rad |
| δ_R | ANRU | Rudder angle | | rad |
| δ_{RF} | ANRF | Rudder-flap angle | | rad |
| λ_R | TARU | Rudder taper | c_T / c_R | 1 |
| λ_{FR} | TAFR | Flanking rudder taper | | 1 |
| λ_R | ASRU | Rudder aspect ratio | b_R^2 / A_{RT} | 1 |
| λ_{FR} | ASRF | Flanking rudder aspect ratio | | |

2.2.3.2 Identifiers for Appendages (Subscripts)

| | |
|----|-----------------|
| BK | Bilge keel |
| BS | Bossing |
| FB | Bow foil |
| FR | Flanking rudder |
| FS | Stern foil |
| KL | Keel |
| RU | Rudder |
| RF | Rudder flap |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------------|------------------------------|-------------|
| | SA | Stabilizer | | |
| | SH | Shafting | | |
| | SK | Skeg | | |
| | ST | Strut | | |
| | TH | Thruster | | |
| | WG | Wedge | | |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

2.2.4 Hydrostatics and Stability

2.2.4.1 Points and Centres (Still under construction)

| | | | | |
|------------------|------|---|---|---|
| A | | Assumed centre of gravity above keel used for cross curves of stability | | |
| b | | Centre of flotation of added buoyant layer or centre of lost buoyancy of the flooded volume | | |
| B | | Centre of buoyancy | Centroid of the underwater volume | |
| F | | Centre of flotation of the water plane | | |
| g | | Centre of gravity of an added or removed weight (mass) | | |
| G | | Centre of gravity of a vessel | | |
| K | | Keel reference | | |
| M | | Metacentre of a vessel | See subscripts for qualification | |
| X_{CB}, L_{CB} | XCB | Longitudinal centre of buoyancy (LCB) | Longitudinal distance from reference point to the centre of buoyancy, B such as X_{MCF} from Midships | m |
| X_{CF}, L_{CF} | XCF | Longitudinal centre of flotation (LCF) | Longitudinal distance from reference point to the centre of flotation, F such as X_{MCF} from Midships | m |
| x_{Cb} | XACB | Longitudinal centre of buoyancy of added buoyant layer | Longitudinal distance from reference point to the centre of buoyancy of the added buoyant layer, b such as x_{MCb} from Midships | m |
| x_{Cf} | XACF | Longitudinal centre of flotation of added buoyant layer | Longitudinal distance from reference point to the centre of flotation of the added buoyant layer, f such as x_{MCf} from Midships | m |
| x_{Cg} | XACG | Longitudinal centre of gravity of added weight (mass) | Longitudinal distance from reference to the centre of gravity, g , of an added or removed weight (mass) such as x_{MCg} from Midships | m |
| X_{CG}, L_{CG} | XCG | Longitudinal centre of gravity (LCG) | Longitudinal distance from a reference point to the centre of gravity, G such as X_{MCG} from Midships | m |
| Y_{CG} | YCG | Lateral displacement of centre of gravity (YCG) | Lateral distance from a reference point to the centre of gravity, G | m |
| Z | ZRA | Intersection of righting arm with line of action of the centre of buoyancy | | |

2.2.4.2 Static Stability levers

| | | | | |
|-----------------|-----|--|---|---|
| \overline{AB} | XAB | Longitudinal centre of buoyancy from aft perpendicular | Distance of centre of buoyancy from aft perpendicular | m |
| \overline{AF} | XAF | Distance of centre of flotation from aft perpendicular | | m |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|------------------------------------|-----------------|---|--|---------|
| \overline{AG}_L | XAG | Longitudinal centre of gravity from aft perpendicular | Distance of centre of gravity from aft perpendicular | m |
| \overline{AG}_T | YAG | Transverse distance from assumed centre of gravity A, to actual centre of gravity G | | m |
| \overline{AG}_V | ZAG | Vertical distance from assumed centre of gravity A, to actual centre of gravity G | | m |
| \overline{AZ} | YAZ | Righting arm based on horizontal distance from assumed centre of gravity A, to Z | Generally tabulated in cross curves of stability | m |
| \overline{BM} | ZBM | Transverse metacentre above centre of buoyancy | Distance from the centre of buoyancy B to the transverse metacentre M. $\overline{BM} = I_T / \nabla = \overline{KM} - \overline{KB}$ | m |
| \overline{BM}_L | ZBML | Longitudinal metacentre above centre of buoyancy | $\overline{KM}_L - \overline{KB}$ | |
| \overline{FB} | XFB | Longitudinal centre of buoyancy, L_{CB} , from forward perpendicular | Distance of centre of buoyancy from forward perpendicular | m |
| \overline{FF} | XFF | Longitudinal centre of floatation, L_{CF} , from forward perpendicular | Distance of centre of flotation from forward perpendicular | m |
| \overline{FG} | XFG | Longitudinal centre of gravity from forward perpendicular | Distance of centre of gravity from forward perpendicular | m |
| \overline{GG}_H | GGH | Horizontal stability lever caused by a weight shift or weight addition | | m |
| \overline{GG}_L | GGL | Longitudinal stability lever caused by a weight shift or weight addition | | m |
| $\overline{GG}_1, \overline{GG}_V$ | GG1, GGV | Vertical stability lever caused by a weight shift or weight addition | $\overline{KG}_1 = \overline{KG}_0 + \overline{GG}_1$ | m |
| \overline{GM} | GM | Transverse metacentric height | Distance of centre of gravity to the metacentre $\overline{KM} - \overline{KG}$ | m |
| \overline{GM}_{EFF} | GMEFF | Effective transverse metacentric height | \overline{GM} corrected for free surface and/or free communication effects | m |
| \overline{GM}_L | GML | Longitudinal centre of metacentric height | Distance from the centre of gravity G to the longitudinal metacentre M_L $\overline{GM}_L = \overline{KM}_L - \overline{KG}$ | m |
| \overline{GZ} | GZ | Righting arm or lever | $\overline{GZ} = \overline{AZ} - \overline{AG}_V \sin \varphi - \overline{AG}_T \cos \varphi$ | m |
| \overline{GZ}_{MAX} | GZMAX | Maximum righting arm or lever | | m |
| \overline{KA} | ZKA | Assumed centre of gravity above moulded base or keel | Distance from the assumed centre of gravity A to the moulded base or keel K | m |
| \overline{KB} | ZKB | Centre of buoyancy above moulded base or keel | Distance from the centre of buoyancy B to the moulded base or keel K | m |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------------|-----------------|--|---|---------|
| \overline{KG} | ZKG | Centre of gravity above moulded base or keel | Distance from centre of gravity G to the moulded base or keel K | m |
| \overline{Kg} | ZKAG | Vertical centre of gravity of added or removed weight above moulded base or keel | Distance from centre of gravity, g, to the moulded base or keel K | m |
| \overline{KM} | ZKM | Transverse metacentre above moulded base or keel | Distance from the transverse metacentre M to the moulded base or keel K | m |
| \overline{KM}_L | ZKML | Longitudinal metacentre above moulded base or keel | Distance from the longitudinal metacentre M_L to the moulded base or keel K | m |
| l | XTA | Longitudinal trimming arm | $x_{CG} - x_{CB}$ | m |
| t | YHA | Equivalent transverse heeling arm | Heeling moment / Δ | m |

2.2.4.3 Derived Quantities

| | | | | |
|-----------|------|---|--|---|
| C_{GM} | CGM | Dimensionless \overline{GM} coefficient | $\overline{GM} / \nabla^{1/3}$ | 1 |
| C_{GZ} | CGZ | Dimensionless \overline{GZ} coefficient | $\overline{GZ} / \nabla^{1/3}$ | 1 |
| C_{KG} | CKG | Dimensionless \overline{KG} coefficient | \overline{KG} / T | 1 |
| C_{MTL} | CMTL | Longitudinal trimming coefficient | Trimming moment divided by change in trim which approximately equals \overline{BM}_L / L | 1 |

2.2.4.4 Intact and Damage (Flooded) Stability

| | | | | |
|------------------|---------|---|--|----------------|
| C_{MTL} | CMTL | Longitudinal trimming coefficient | trimming moment divided by change in trim which approximately equals \overline{BM}_L / L | 1 |
| f | FREB | Freeboard | From the freeboard markings to the freeboard deck, according to official rules | m |
| A_{SI}, I_{AS} | ASI | Attained subdivision index | (to be clarified) | 1 |
| M_S | MS | Moment of ship stability in general | $\Delta \overline{GZ}$ Other moments such as those of capsizing, heeling, etc. will be represented by MS with additional subscripts as appropriate | Nm |
| m | SHIPMA | Ship mass | W / g | kg |
| M_{TC} | MTC | Moment to change trim by one centimetre | | Nm/cm |
| M_{TM} | MTM | Moment to change trim by one meter | ΔC_{MTL} | Nm/m |
| R_{SI} | RSI | Required subdivision index | | 1 |
| t_s, t_{KL} | TRIM | Static trim | $T_A - T_F - d_{KL}$ | m |
| W | SHIPWT | Ship weight | $m g$ | N |
| z_{SF} | ZSF | Static sinkage at FP | Caused by loading | m |
| z_{SA} | ZSA | Static sinkage at AP | Caused by loading | m |
| z_S | ZS | Mean static sinkage | $(z_{SF} + z_{SA}) / 2$ | m |
| δ | D | Finite increment in... | Prefix to other symbol | 1 |
| δt_{KL} | DTR | Change in static trim | | m |
| Δ | DISPF | Displacement (buoyant) force | $g \rho \nabla$ | N |
| Δ_m | DISPM | Displacement mass | $\rho \nabla$ | kg |
| ∇ | DISPVOL | Displacement volume | $\Delta / (\rho g)$ | m ³ |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|--------------------------------------|---|----------------|
| V_{fw} | DISVOLFW | Displacement volume of flooded water | $\Delta f_w / (\rho g)$ | m ³ |
| θ_s | TRIMS | Static trim angle | $\tan^{-1}((z_{SF} - z_{SA}) / L)$ | rad |
| μ | PMVO | Volumetric permeability | The ratio of the volume of flooding water in a compartment to the total volume of the compartment | 1 |
| ϕ | HEELANG | Heel angle | | rad |
| ϕ_F | HEELANGF | Heel angle at flooding | | rad |
| ϕ_{vs} | HEELANGV | Heel angle for vanishing stability | | rad |

2.2.4.5 Symbols for Attributes and Subscripts (under construction)

| | |
|---------------|------------------------------|
| a | apparent |
| A, att | attained |
| d, dyn | dynamic |
| e, EFF | effective |
| f | false |
| KL | keel line |
| L | longitudinal |
| MAX | maximum |
| MTL | longitudinal trimming moment |
| R, req | required (to be clarified) |
| s | Static |
| S, <i>sqt</i> | Sinkage, squat |
| TC | Trim in cm |
| TM | Trim in m |
| T | transverse |
| V | vertical |
| 0 | Initial |
| ϕ | at heel angle ϕ |
| θ | at trim angle θ |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

2.3 Resistance and Propulsion

2.3.1 Hull Resistance

(see also Section 1.4.1 on Waves)

2.3.1.1 Basic Quantities

| | | | | |
|--------------|-------|---|---|----------------|
| m | BLCK | Blockage parameter | Maximum transverse area of model ship divided by tank cross section area | 1 |
| R_A | RA | Model-ship correlation allowance | Incremental resistance to be added to the smooth ship resistance to complete the model-ship prediction | N |
| R_{AA} | RAA | Air or wind resistance | | N |
| R_{APP} | RAP | Appendage resistance | | N |
| R_{AR} | RAR | Roughness resistance | | N |
| R_C | RC | Resistance corrected for difference in temperature between resistance and self-propulsion tests | $R_{TM}[(1+k)C_{FMC} + C_R] / [(1+k)C_{FM} + C_R]$ where C_{FMC} is the frictional coefficient at the temperature of the self-propulsion test | N |
| R_F | RF | Frictional resistance of a body | Due to fluid friction on the surface of the body | N |
| R_{F0} | RF0 | Frictional resistance of a flat plate | | N |
| R_P | RP | Pressure resistance | Due to the normal stresses over the surface of a body | N |
| R_{PV} | RPV | Viscous pressure resistance | Due to normal stress related to viscosity and turbulence | N |
| R_R | RR | Residuary resistance | $R_T - R_F$ or $R_T - R_{F0}$ | N |
| R_{RBH} | RRBH | Residuary resistance of the bare hull | | N |
| R_S | RS | Spray resistance | Due to generation of spray | N |
| R_T | RT | Total resistance | Total towed resistance | N |
| R_{TBH} | RTBH | Total resistance of bare hull | | N |
| R_V | RV | Total viscous resistance | $R_F + R_{PV}$ | N |
| R_W | RW | Wave making resistance | Due to formation of surface waves | N |
| R_{WB} | RWB | Wave breaking resistance | Associated with the breakdown of the bow wave | N |
| R_{WP} | RWP | Wave pattern resistance | | N |
| S | S | Wetted surface area, underway | $S_{BH} + S_{APP}$ | m ² |
| S_0 | S0 | Wetted surface area, at rest | $S_{BH0} + S_{APP0}$ | m ² |
| S_{APP} | SAP | Appendage wetted surface area, underway | | m ² |
| S_{APP0} | SAP0 | Appendage wetted surface area, at rest | | m ² |
| S_{BH} | SBH | Bare Hull wetted surface area, underway | | m ² |
| S_{BH0} | SBH0 | Bare Hull wetted surface area, at rest | | m ² |
| ΔC_F | DELCF | Roughness allowance | | 1 |
| V | V | Speed of the model or the ship | | m/s |
| V_K | VKN | Speed in knots | | |
| V_{WR} | VWR | Wind velocity, relative | | m/s |
| z_{VF} | ZVF | Running sinkage at FP | | m |
| z_{VA} | ZVA | Running sinkage at AP | | m |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|----------------------|-----------------|------------------------------|------------------------------------|-------------------|
| z_{VM} | ZVM | Mean running sinkage | $(z_{VF} + z_{VA}) / 2$ | m |
| η | EW | Wave Elevation | see 3.4.1 | m |
| θ_V, θ_D | TRIMV | Running (dynamic) trim angle | $\tan^{-1}((z_{VF} - z_{VA}) / L)$ | 1 |
| τ_W | LSF, TAUW | Local skin friction | see 3.3.4 | N/ m ² |

2.3.1.2 Derived Quantities

| | | | | |
|-------------|--------|---|---|----|
| C_A | CA | Incremental resistance coefficient for model ship correlation | $R_A / (S q)$ | 1 |
| C_{AA} | CAA | Air or wind resistance coefficient | $R_{AA} / (S q)$ $= C_{DA} \frac{\rho_A}{\rho_S} \frac{A_V}{S_S} = -C_X \frac{\rho_A}{\rho_S} \frac{A_V}{S_S}$ | 1 |
| C_{APP} | CAPP | Appendage resistance coefficient | $R_{APP} / (S q)$ | 1 |
| C_D | CD | Drag coefficient | $D / (S q)$ | 1 |
| C_{DA} | CDA | Fujiwara air or wind resistance coefficient, from wind tunnel tests | $R_{AA} / (A_V q_R)$ | 1 |
| C_F | CF | Frictional resistance coefficient of a body | $R_F / (S q)$ | 1 |
| C_{F0} | CF0 | Frictional resistance coefficient of a corresponding plate | $R_{F0} / (S q)$ | 1 |
| C_p | CP | Local pressure coefficient | | 1 |
| C_{PR} | CPR | Pressure resistance coefficient, including wave effect | $R_P / (S q)$ | 1 |
| C_{PV} | CPV | Viscous pressure resistance coefficient | $R_{PV} / (S q)$ | 1 |
| C_R | CR | Residuary resistance coefficient | $R_R / (S q)$ | 1 |
| C_S | CSR | Spray resistance coefficient | $R_S / (S q)$ | 1 |
| C_T | CT | Total resistance coefficient | $R_T / (S q)$ | 1 |
| C_{TL} | CTLT | Telfer's resistance coefficient | $g R L / (\Delta V^2)$ | 1 |
| C_{TQ} | CTQ | Qualified resistance coefficient | $C_{TV} / (\eta_H \eta_R)$ | 1 |
| C_{TV} | CTVOL | Resistance displacement | $R_T / (V^{2/3} q)$ | 1 |
| C_V | CV | Total viscous resistance coefficient | $R_V / (S q)$ | 1 |
| C_W | CW | Wave making resistance coefficient | $R_W / (S q)$ | 1 |
| C_{WP} | CWP | Wave pattern resistance coefficient, by wave analysis | | 1 |
| C_X | CXA | Air or wind resistance coefficient, usually from wind tunnel tests | $-R_{AA} / (A_V q_R)$ | 1 |
| C^C | CIRCC | R.E. Froude's resistance coefficient | $1000 R_T / (\Delta (K^C)^2)$ | 1 |
| F^C | CIRCF | R.E. Froude's frictional resistance coefficient | $1000 R_F / (\Delta (K^C)^2)$ | 1 |
| f | FC | Friction coefficient | Ratio of tangential force to normal force between two sliding bodies | 1 |
| k | K | Three dimensional form factor on flat plate friction | $(C_V - C_{F0}) / C_{F0}$ | 1 |
| $k(\theta)$ | WDC | Wind direction coefficient | C_{AA} / C_{AA0} | 1 |
| K^C | CIRCK | R.E. Froude's speed displacement coefficient | $(4 \pi)^{1/2} Fr_V$ or $(4 \pi / g)^{1/2} V_K / V^{1/6}$ | |
| K_R | KR | Resistance coefficient corresponding to K_Q, K_T | $R / (\rho D^4 n^2)$ | 1 |
| q | PD, EK | Dynamic pressure, density of kinetic flow energy, | $\rho V^2 / 2$ see 3.3.2 | Pa |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|-----------------|--------------------|---|----------------------------------|-------------|
| q_R | PDWR, EKWR | Dynamic pressure based on apparent wind | $\rho V_{WR}^2 / 2$ see 3.4.2 | Pa |
| S^C | CIRCS | R. E. Froude's wetted surface coefficient | $S / \nabla^{2/3}$ | 1 |
| ε | EPSG | Resistance-displacement ratio in general | R / Δ | 1 |
| ε_R | EPSR | Residuary resistance-displacement ratio | R_R / Δ | 1 |

2.3.1.3 Symbols for Attributes and Subscripts

| | |
|----|------------------------|
| FW | Fresh water |
| MF | Faired model data |
| MR | Raw model data |
| OW | Open water |
| SF | Faired full scale data |
| SR | Raw full scale data |
| SW | Salt water |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

2.3.2 Ship Performance

2.3.2.1 Basic Quantities

| | | | | |
|------------|--------|--|--|-----|
| F_D | SFC | Friction deduction force in self propulsion test | Towing force applied to a model to correct the model resistance for different Re between model and full scale. | N |
| F_P | FP | Force pulling or towing a ship | | N |
| F_{P0} | FPO | Pull during bollard test | | N |
| k_S | KHS | Roughness height of Hull surface | | m |
| n | N | Frequency, commonly rate of revolution | | Hz |
| P_B | PB | Brake power | Power delivered by prime mover | W |
| P_D, P_P | PD, PP | Delivered power, propeller power | $Q \omega$ | W |
| P_E, P_R | PE, PR | Effective power, resistance power | $R V$ | W |
| P_I | PI | Indicated power | Determined from pressure measured by indicator | W |
| P_S | PS | Shaft power | Power measured on the shaft | W |
| P_T | PTH | Thrust power | $T V_A$ | W |
| Q | Q | Torque | P_D / ω | Nm |
| t_V | TV | Running trim | | m |
| V | V | Ship speed | | m/s |
| V_A | VA | Propeller advance speed | Equivalent propeller open water speed based on thrust or torque identity | m/s |
| z_V | ZV | Running sinkage of model or ship | | m |
| ω | V0,OMN | Rotational shaft velocity | $2 \pi n$ | 1/s |

2.3.2.2 Derived Quantities

| | | | | |
|----------------|-------|---|---|---|
| a | RAUG | Resistance augment fraction | $(T - R_T) / R_T$ | 1 |
| C_{ADM} | CADM | Admiralty coefficient | $\Delta^{2/3} V^3 / P_S$ | 1 |
| $C_{D \nabla}$ | CDVOL | Power-displacement coefficient | $P_D / (\rho V^3 \nabla^{2/3} / 2)$ | 1 |
| C_N | CN | Trial correction for propeller rate of revolution at speed identity | n_T / n_S | 1 |
| C_{NP} | CNP | Trial correction for propeller rate of revolution at power identity | P_{DT} / P_{DS} | 1 |
| C_P | CDP | Trial correction for delivered power | | 1 |
| K_1 | C1 | Ship model correlation factor for propulsive efficiency | η_{DS} / η_{DM} | 1 |
| K_2 | C2 | Ship model correlation factor for propeller rate revolution | n_S / n_M | 1 |
| K_{APP} | KAP | Appendage correction factor | Scale effect correction factor for model appendage drag applied at the towing force in a self-propulsion test | 1 |
| s_V | SINKV | Sinkage, dynamic | Change of draught, fore and aft, divided by length | 1 |
| t_V | TRIMV | Trim, dynamic | Change of the trim due to dynamic condition, divided by length | 1 |
| t | THDF | Thrust deduction fraction | $(T - R_T) / T$ | 1 |
| w | WFT | Taylor wake fraction in general | $(V - V_A) / V$ | 1 |
| w_F | WFF | Froude wake fraction | $(V - V_A) / V_A$ | 1 |
| w_Q | WFTQ | Torque wake fraction | Propeller speed V_A determined from torque identity | 1 |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|--------------|-----------------|--|---|---------|
| w_T | WFTT | Thrust wake fraction | Propeller speed, V_A , determined from thrust identity | 1 |
| Δw | DELW | Ship-model correlation factor for wake fraction | $w_{T,M} - w_{T,S}$ | 1 |
| Δw_C | DELWC | Ship-model correlation factor with respect to $w_{T,S}$ method formula of ITTC 1978 method | | 1 |
| x | XLO | Load fraction in power prediction | $\eta_D P_D / P_E - 1$ | 1 |
| β | APSF | Appendage scale effect factor | Ship appendage resistance divided by model appendage resistance | 1 |

2.3.2.3 Efficiencies etc.

| | | | | |
|--------------|-------------|--|--|---|
| η_{APP} | ETAAP | Appendage efficiency | $P_{Ew0APP} / P_{EwAPP}, R_{TBH} / R_T$ | 1 |
| η_B | ETAB, EFTP | Propeller efficiency behind ship | $P_T / P_D = T V_A / (Q \omega)$ | 1 |
| η_D | ETAD, EFRP | Quasi-propulsive efficiency coefficient | $P_E / P_D = P_R / P_P$ | 1 |
| η_G | ETAG, EFGP | Gearing efficiency | | 1 |
| η_H | ETAH, EFRT | Hull efficiency | $P_E / P_T = P_R / P_T = (1 - t) / (1 - w)$ | 1 |
| η_M | ETAM | Mechanical efficiency of transmission between engine and propeller | P_D / P_B | 1 |
| η_O | ETAO, EFTPO | Propeller efficiency in open water | $P_T / P_D = T V_A / (Q \omega)$ all quantities measured in open water tests | 1 |
| η_P | ETAP | Propulsive efficiency coefficient | P_E / P_B | 1 |
| η_R | ETAR, EFRO | Relative rotative efficiency | η_B / η_O | 1 |
| η_S | ETAS, EFPS | Shafting efficiency | $P_D / P_S = P_P / P_S$ | 1 |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

2.3.3 Propulsor Performance

2.3.3.1 Basic Quantities

| | | | | |
|----------|------|--|---|-------------------|
| A_O | AO | Propeller disc area | $\pi D^2 / 4$ | m ² |
| D | DP | Propeller diameter | | m |
| n | FR | Propeller frequency of revolution | | Hz |
| k_P | KS | Roughness height of propeller blade surface | | m |
| q_A | QA | Dynamic pressure based on advance speed | $\rho V_A^2 / 2$ | Pa |
| q_S | QS | Dynamic pressure based on section advance speed | $\rho V_S^2 / 2$ | Pa |
| Q_S | QSP | Spindle torque | About spindle axis of controllable pitch propeller $Q_S = Q_{SC} + Q_{SH}$ positive if it increases pitch | Nm |
| Q_{SC} | QSPC | Centrifugal spindle torque | | Nm |
| Q_{SH} | QSPH | Hydrodynamic spindle torque | | Nm |
| R_U | RU | Pod unit resistance | Resistance of a podded drive unit | N |
| T | TH | Propeller thrust | | N |
| T_U | TU | Pod unit thrust | Pod unit resistance subtracted from the propeller thrust | N |
| T_D | THDU | Duct thrust | | N |
| T_{DP} | THDP | Ducted propeller thrust | | N |
| T_{DT} | THDT | Total thrust of a ducted propeller unit | | N |
| T_{xP} | TXP | Propeller Thrust along shaft axis | | N |
| T_{yP} | TYP | Propeller normal force in y direction in propeller axis | | N |
| T_{zP} | TZP | Propeller normal force in z direction in propeller axis | | N |
| V_A | VA | Advance speed of propeller | | m/s |
| V_P | VP | Mean axial velocity at propeller plane of ducted propeller | | m/s |
| V_S | VS | Section advance speed at 0.7 R | $(V_A^2 + (0.7 R \omega)^2)^{1/2}$ | m/s |
| ρ_P | DNP | Propeller mass density | | kg/m ³ |
| ω | VOP | Propeller rotational velocity | $2 \pi n$ | 1/s |

2.3.3.2 Derived Quantities

| | | | | |
|------------|--------|--|---|---|
| B_P | BP | Taylor's propeller coefficient based on delivered horsepower | $n P_D^{1/2} / V_A^{2.5}$ with n in revs/min, P_D in horsepower, and V_A in kn (obsolete) | 1 |
| B_U | BU | Taylor's propeller coefficient based on thrust horsepower | $n P_T^{1/2} / V_A^{2.5}$ with n in revs/min, P_T in horsepower, and V_A in kn (obsolete) | 1 |
| C_P | CPD | Power loading coefficient | $P_D / (A_P q_A V_A)$ | 1 |
| C_{Q^*} | CQS | Torque index | $Q / (A_P q_S D)$ | 1 |
| C_{Th} | CTH | Thrust loading coefficient, energy loading coefficient | $T / (A_P q_A) = (T_P / A_P) / q_A$ | 1 |
| C_{T^*} | CTHS | Thrust index | $T / (A_P q_S)$ | 1 |
| J | JEI | Propeller advance ratio | $V_A / (D n)$ | 1 |
| J_A, J_H | JA, JH | Apparent or hull advance ratio | $V / (D n) = V_H / (D n)$ | 1 |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|----------------------|-----------------|--|--|---------|
| J_P | JP | Propeller advance ratio for ducted propeller | $V_P / (D n)$ | |
| J_T, J_{PT} | JT, JPT | Advance ratio of propeller determined from thrust identity | | 1 |
| J_Q, J_{PQ} | JQ, JPQ | Advance ratio of propeller determined from torque identity | | 1 |
| K_P | KP | Delivered power coefficient | $P_D / (\rho n^3 D^5) = 2 \pi K_Q$ | 1 |
| K_Q | KQ | Torque coefficient | $Q / (\rho n^2 D^5)$ | 1 |
| K_{SC} | KSC | Centrifugal spindle torque coefficient | $Q_{SC} / (\rho n^2 D^5)$ | 1 |
| K_{SH} | KSH | Hydrodynamic spindle torque coefficient | $Q_{SH} / (\rho n^2 D^5)$ | 1 |
| K_T | KT | Thrust coefficient | $T / (\rho n^2 D^4)$ | 1 |
| K_{TD} | KTD | Duct thrust coefficient | $T_D / (\rho n^2 D^4)$ | 1 |
| K_{TP} | KTP | Ducted propeller thrust coefficient | $T_P / (\rho n^2 D^4)$ | 1 |
| K_{TT} | KT | Total thrust coefficient for a ducted propeller unit | $K_{TP} + K_{TD}$ | 1 |
| K_{Q0} | KQ0 | Torque coefficient of propeller converted from behind to open water condition | $K_Q \eta_R$ | 1 |
| K_{QT} | KQT | Torque coefficient of propeller determined from thrust coefficient identity | | 1 |
| P_J | PJ | Propeller jet power | $\eta_{TJ} T V_A$ | |
| S_A | SRA | Apparent slip ratio | $1 - V / (n P)$ | 1 |
| S_R | SRR | Real slip ratio | $1 - V_A / (n P)$ | 1 |
| δ | ADCT | Taylor's advance coefficient | $n D / V_A$ with n in revs/min, D in feet, V_A in kn | 1 |
| η_{JP} | EFJP | Propeller pump or hydraulic efficiency | $P_J / P_D = P_J / P_P$ | 1 |
| η_{JP0} | ZET0, EFJP0 | Propeller pump efficiency at zero advance speed, alias static thrust coefficient | $T / (\rho \pi / 2)^{1/3} / (P_D D)^{2/3}$ | 1 |
| η_I | EFID | Ideal propeller efficiency | Efficiency in non-viscous fluid | 1 |
| η_{TJ} | EFTJ | Propeller jet efficiency | $2 / (1 + (1 + C_{T0})^{1/2})$ | 1 |
| η_0, η_{TP0} | ETA0, EFTP0 | Propeller efficiency in open water | $P_T / P_D = T V_A / (Q \omega)$ all quantities measured in open water tests | 1 |
| λ | ADR | Advance ratio of a propeller | $V_A / (n D) / \pi = J / \pi$ | 1 |
| τ | TMR | Ratio between propeller thrust and total thrust of ducted propeller | T_P / T_T | 1 |

2.3.3.3 Induced Velocities etc.

| | | | | |
|----------|------|--|--|-----|
| U_A | UA | Axial velocity induced by propeller | | m/s |
| U_{AD} | UADU | Axial velocity induced by duct of ducted propeller | | m/s |
| U_{RP} | URP | Radial velocity induced by propeller of ducted propeller | | m/s |
| U_{RD} | URDU | Radial velocity induced by duct of ducted propeller | | m/s |
| U_{AP} | UAP | Axial velocity induced by propeller of ducted propeller | | m/s |
| U_R | UR | Radial velocity induced by propeller | | m/s |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|--|---|-------------|
| U_{TD} | UTDU | Tangential velocity induced by duct of ducted propeller | | m/s |
| U_{TP} | UTP | Tangential velocity induced by propeller of ducted propeller | | m/s |
| U_T | UT | Tangential velocity induced by propeller | | m/s |
| β | BETB | Advance angle of a propeller blade section | $\arctg(V_A / r \omega)$ | rad |
| β_I | BETI | Hydrodynamic flow angle of a propeller blade section | Flow angle taking into account induced velocity | rad |
| β^* | BETS | Effective advance angle | $\arctg(V_A / (0.7 R \omega))$ | rad |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

2.3.4 Unsteady Propeller Forces

2.3.4.1 Basic Quantities

| | | | | |
|-------------------|---------------|--|--|--|
| C_{uv} | SI(U,V) | Generalized stiffness | | |
| D_{uv} | DA(U,V) | Generalized damping | | |
| F_u | FG(I) | Generalized vibratory force | $u = 1, \dots, 6$ $u = 1, 2, 3$: force $u = 4, 5, 6$: moment | N N Nm |
| F_i | F(I) | Vibratory force | $i = 1, 2, 3$ | N |
| K_{Fu} | KF(U) | Generalized vibratory force coefficients | According to definitions of K_{Fi} and K_{Mi} | 1 |
| K_{Fi} | KF(I) | Vibratory force coefficients | $F_i / (\rho n^2 D^4)$ | 1 |
| K_{Mi} | KM(I) | Vibratory moment coefficients | $M_i / (\rho n^2 D^5)$ | 1 |
| K_p | KPR | Pressure coefficient | $p / (\rho n^2 D^2)$ | 1 |
| M_i | M(I) | Vibratory moment | $i = 1, 2, 3$ | Nm |
| M_{uv} | MA(U,V) | Generalized mass | | |
| p | PR | Pressure | | Pa |
| R_u | R(U) | Generalized vibratory bearing reaction | $u = 1, \dots, 6$ $u = 1, 2, 3$: force $u = 4, 5, 6$: moment | N N Nm |
| V_i | V(I) | Velocity field of the wake | $i = 1, 2, 3$ | m/s |
| x y z | X Y Z | Cartesian coordinates | Origin O coinciding with the centre of the propeller. The longitudinal x -axis coincides with the shaft axis, positive forward; the transverse y -axis, positive to port; the third, z -axis, positive upward | m m m |
| X a r | X ATT R | Cylindrical coordinates | Cylindrical system with origin O and longitudinal x -axis as defined before; angular a -(attitude)-coordinate, zero at 12 o'clock position, positive clockwise looking forward; r distance measured from the x -axis | m 1 m |
| δ_u | DP(U) | Generalized vibratory displacement | $u = 1, \dots, 6$ $u = 1, 2, 3$: linear $u = 4, 5, 6$: angular | m m rad |
| $\dot{\delta}_u$ | DPVL(U) | Generalized vibratory velocity | $u = 1, \dots, 6$ $u = 1, 2, 3$: linear $u = 4, 5, 6$: angular | m/s m/s rad/s |
| $\ddot{\delta}_u$ | DPAC(U) | Generalized vibratory acceleration | $u = 1, \dots, 6$ $u = 1, 2, 3$: linear $u = 4, 5, 6$: angular | m/s ² m/s ² rad/s ² |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

2.3.5 Water Jets

| | | | | |
|---------------------|-----|--|--|----|
| C_p | CP | Local pressure coefficient | $(p-p_0)/(\rho V^2/2)$ | 1 |
| C_{Tn} | | Thrust loading coefficient:viscous pressure | $\frac{T_{net}}{\frac{1}{2} \rho U_0^2 A_n}$ | 1 |
| c_{es} | | Energy velocity coefficient at station s | | 1 |
| c_{ms} | | Momentum velocity coefficient at station s | | 1 |
| Dp | | Pressure differential of flow rate transducer | | Pa |
| E_j | EJ | Energy flux at station j | $E_j = (\rho/2) \int V_{Ej}^2 dQ_j$ | W |
| E_s | | Total energy flux at station s (kinetic + potential + pressure) | $\iint_{A_s} \rho \left(\frac{1}{2} \mathbf{u}^2 + \frac{p}{\rho} - g_j x_j \right) u_i n_i dA$ | W |
| $E_{s\xi}$ | | Total axial (in ξ direction) energy flux at station s | $\iint_{A_s} \rho \left(\frac{1}{2} u_\xi^2 + \frac{p}{\rho} - g_j x_j \right) u_i n_i dA$ | W |
| F_D | | Skin friction correction in a self propulsion test carried out at the ship self-propulsion point | | N |
| H_1 | HT1 | Local total head at station 1 | | m |
| H_{35} | H35 | Mean increase of total head across pump and stator or several pump stages | | m |
| I_{VR} | IVR | Intake velocity ratio | VI/V | 1 |
| J_{VR} | JVR | Jet velocity ratio | VJ/V | 1 |
| K_Q | | Impeller torque coefficient: | $\frac{Q}{\rho n^2 D^5}$ | |
| K_{QJ} | | Flow rate coefficient: | $\frac{Q_j}{n D^3}$ | 1 |
| \overline{M}_{is} | | Momentum flux at station s in i direction | $\iint_{A_s} \rho u_i (u_j n_j) dA$ | N |
| NVR | | Nozzle velocity ratio: | $\frac{\overline{u_{6\xi}}}{U_0}$ | 1 |
| T_{jx} | TJX | Jet thrust (can be measured directly in bollard pull condition) | | N |
| n | | Impeller rotation rate | | Hz |
| n_i | | Unit normal vector in i direction | | 1 |
| P_D | | Delivered Power to pump impeller | | W |
| P_E | | Effective power: | $R_{TBH} U_0$ | W |
| P_{JSE} | | Effective Jet System Power | $Q_J H_{1A7}$ | W |
| P_{PE} | | Pump effective power: | $Q_J H_{35}$ | W |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------------------|-----------------|--|---|-------------------|
| P_{TE} | | Effective thrust power | | W |
| p_0 | PR0 | Ambient pressure in undisturbed flow | | Pa |
| p_s | | Local static pressure at station s | | Pa |
| Q | | Impeller torque | | Nm |
| Q_{bl} | | Volume flow rate inside boundary layer | | m ³ /s |
| Q_j | | Volume flow rate through water jet system | | m ³ /s |
| R_{TBH} | | Total resistance of bare hull | | N |
| $T_{jet.x}$ | | Jet thrust (can be measured directly in bollard pull condition) | | N |
| T_{net} | | Net thrust exerted by the jet system on the hull | | N |
| t | | Thrust deduction fraction | $(1-t) = \frac{R_{TBH}}{T_{net}}$ | 1 |
| U_0 | | Free stream velocity | | m/s |
| $\overline{u_{eis}}$ | | Mean energy velocity in i direction at station s | $\sqrt{\frac{1}{Q_j} \iint u_{\xi}^3 dA}$ | m/s |
| $\overline{u_{es}}$ | | Mean (total) energy velocity at station s | $\sqrt{\frac{1}{Q_j} \iint u^3 dA}$ | m/s |
| u_{is} | | Velocity component in i -direction at station s | | m/s |
| u_s | | Velocity at station s | | m/s |
| $u_{7\phi}$ | UJFI | Local tangential velocity at station 7 | | m/s |
| w_1 | | Geometric intake width at station 1 | | m |
| w_{1A} | | Width of capture area measured over hull surface at station 1A | | m |
| z_6 | | Vertical distance of nozzle centre relative to undisturbed surface | | m |
| ΔM | DMF | Change of momentum flux | | N |
| $\Delta \overline{M}_x$ | | Change in Momentum Flux in x direction | | N |
| η_D | | Overall propulsive efficiency: | $\frac{P_E}{P_D}$ | 1 |
| η_{duct} | | Ducting efficiency: | $\frac{P_{JSE}}{P_{PE}}$ | 1 |
| η_{el} | | Energy interaction efficiency: | $\frac{P_{JSE0}}{P_{JSE}}$ | 1 |
| η_I | | Ideal efficiency, equivalent to jet efficiency in free stream conditions | $\frac{P_{TE0}}{P_{JSE0}}$ | 1 |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|----------------------|-----------------|---|--|-------------------|
| η_{inst} | | Installation efficiency to account for the distorted flow delivered by the jet intake to the pump | | 1 |
| η_{INT} | | Total interaction efficiency: | $\frac{\eta_{\text{el}}}{\eta_{\text{ml}}} (1 - t)$ | 1 |
| η_{jet} | | Momentum or jet efficiency: | $\frac{P_{\text{TE}}}{P_{\text{JSE}}}$ | 1 |
| η_{JS} | | Jet system efficiency: | $\frac{P_{\text{JSE}}}{P_{\text{D}}}$ | 1 |
| η_{ml} | | Momentum interaction efficiency: | $\frac{T_{\text{net0}}}{T_{\text{net}}}$ | 1 |
| η_{P} | ETAP | Pump efficiency | $\frac{P_{\text{PE}}}{P_{\text{D}}}$ | 1 |
| η_{P0} | | Pump efficiency from a pump loop test | | 1 |
| η_0 | | Free stream efficiency: | $\eta_{\text{P}} \eta_{\text{duct}} \eta_{\text{I}}$ | 1 |
| θ_{n} | | Jet angle relative to the horizontal at the nozzle (station 6) | | rad |
| ρ | | Mass density of fluid | | kg/m ³ |
| ζ_{ij} | | Energy loss coefficient between station i and j | | 1 |
| ζ_{13} | ZETA13 | Inlet duct loss coefficient: | $\frac{E_3 - E_1}{\frac{1}{2} \rho U_0^2}$ | 1 |
| ζ_{57} | ZETA57 | Nozzle duct loss coefficient: | $\frac{E_7 - E_5}{\frac{1}{2} \rho u_{\text{e6}}^2}$ | 1 |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

2.4 Manoeuvrability and Sea Keeping

2.4.1 Manoeuvrability

2.4.1.1 Geometrical Quantities

see also Section 1.3.1 and Section 1.3.3

| | | | | |
|------------|--------|--|---|----------------|
| A_{FB} | AFBO | Projected area of bow fins | | m ² |
| A_{HL} | AHLT | Lateral area of the hull | The area of the profile of the underwater hull of a ship when projected normally upon the longitudinal centre plane | m ² |
| A_{LV} | AHLV | Lateral area of hull above water | | m ² |
| A_R | ARU | Total lateral area of rudder | | m ² |
| A_{Rmov} | ARMV | Lateral area of movable part of rudder | | m ² |
| A_{RN} | ARNO | Nominal lateral area of rudder | $(A_R + A_{Rmov}) / 2$ | m ² |
| b_R | SPRU | Rudder span | Maximum distance from root to tip | m |
| b_{RM} | SPRUME | Mean span of rudder | | m |
| C_{AL} | CAHL | Coefficient of lateral area of ship | $A_{HL} / (L T)$ | 1 |
| h | DE | Water depth | | m |
| h_M | DEME | Mean water depth | | m |
| x_R | XRU | Longitudinal position of rudder axis | | m |
| δ | ANRU | Rudder angle, helm angle | | rad |
| A_R | ASRU | Aspect ratio of rudder | b_R^2 / A_R | 1 |

2.4.1.2 Motions and Attitudes

| | | | | |
|------------|----------|---|-----------|------------------|
| p | OX, P | Roll velocity, rotational velocity about body x -axis | | 1/s |
| q | OY, Q | Pitch velocity, rotational velocity about body y -axis | | 1/s |
| r | OZ, R | Yaw velocity, rotational velocity about body z -axis | | 1/s |
| \dot{p} | OXRT, PR | Roll acceleration, angular acceleration about body x -axis | dp / dt | 1/s ² |
| \dot{q} | OYRT, QR | Pitch acceleration, angular acceleration about body y -axis | dq / dt | 1/s ² |
| \dot{r} | OZRT, RR | Yaw acceleration, angular acceleration about body z -axis | dr / dt | 1/s ² |
| u | UX, U | Surge velocity, linear velocity along body x -axis | | m/s |
| v | UY, V | Sway velocity, linear velocity along body y -axis | | m/s |
| w | UZ, W | Heave velocity, linear velocity along body z -axis | | m/s |
| \dot{u} | UXRT, UR | Surge acceleration, linear acceleration along body x -axis | du / dt | m/s ² |
| \dot{v} | UYRT, VR | Sway acceleration, linear acceleration along body y -axis | dv / dt | m/s ² |
| \dot{w} | UZRT, WR | Heave acceleration, linear acceleration along body z -axis | dw / dt | m/s ² |
| V | V | Linear velocity of origin in body axes | | m/s |
| V_A, V_0 | VA, V0 | Approach speed | | m/s |
| V_u | V(URT) | Generalized velocity | | m/s |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|--------------------------|---------------------------|------------------|
| \dot{V}_u | V(URT) | Generalized acceleration | | m/s ² |
| V_F | VF | Flow or current velocity | | m/s |
| V_{WR} | VWREL | Relative wind velocity | | m/s |
| V_{WT} | VWABS | True wind velocity | | m/s |
| ψ | YA | Course angle or heading | | rad |
| χ | YX | Yaw angle | | rad |
| d_{ψ} | YART | Rate of change of course | $d\psi / dt$ | rad/s |
| Ψ_O | YA0R | Original course | | rad |
| θ | PI | Pitch angle | | rad |
| ϕ | RO | Roll angle | | rad |

2.4.1.3 Flow Angles etc.

| | | | | |
|----------------|--------|--|--------------------------------------|-----|
| α | AAPI | Pitch angle | Angle of attack in pitch on the hull | rad |
| β | AADR | Drift angle | Angle of attack in yaw on the hull | rad |
| β_{WR} | ANWIRL | Angle of attack of relative wind | | rad |
| δ | ANCS | Angle of a control surface, rudder angle, helm angle | | rad |
| δ_0 | ANRU0 | Neutral rudder angle | | rad |
| δ_{EFF} | ANRUEF | Effective rudder inflow angle | | rad |
| δ_{FB} | ANFB | Bow fin angle | | rad |
| δ_{FS} | ANFS | Stern fin angle | | rad |
| δ_R | ANRU | Rudder angle | | rad |
| δ_{RO} | ANRUOR | Rudder angle, ordered | | rad |
| ψ_C | COCU | Course of current velocity | | rad |
| ψ_{WA} | COWIAB | Absolute wind direction | see also section 3.4.2, Wind | rad |
| ψ_{WR} | COWIRL | Relative wind direction | | rad |

2.4.1.4 Forces and Derivatives

| | | | | |
|---------------|------|--|---------------------------------|------------------|
| K | MX | Roll moment on body, moment about body x -axis | | Nm |
| M | MY | Pitch moment on body, moment about body y -axis | | Nm |
| N | MZ | Yaw moment on body, moment about body z -axis | | Nm |
| N_r | NR | Derivative of yaw moment with respect to yaw velocity | $\partial N / \partial r$ | Nms |
| $N_{\dot{r}}$ | NRRT | Derivative of yaw moment with respect to yaw acceleration | $\partial N / \partial \dot{r}$ | Nms ² |
| N_v | NV | Derivative of yaw moment with respect to sway velocity | $\partial N / \partial v$ | Ns |
| $N_{\dot{v}}$ | NVRT | Derivative of yaw moment with respect to sway acceleration | $\partial N / \partial \dot{v}$ | Nms ² |
| N_{δ} | ND | Derivative of yaw moment with respect to rudder angle | $\partial N / \partial \delta$ | Nm |
| Q_{FB} | QFB | Torque of bow fin | | Nm |
| Q_R | QRU | Torque about rudder stock | | Nm |
| Q_{FS} | QFS | Torque of stern fin | | Nm |
| X | FX | Surge force on body, force along body x -axis | | N |
| X_R | XRU | Longitudinal rudder force | | N |
| X_u | XU | Derivative of surge force with respect to surge velocity | $\partial X / \partial u$ | Ns/m |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|---------------|-----------------|--|---------------------------------|--------------------|
| $X_{\dot{u}}$ | XURT | Derivative of surge force with respect to surge acceleration | $\partial X / \partial \dot{u}$ | Ns ² /m |
| Y | FY | Sway force, force in direction of body axis y | | N |
| Y_r | YR | Derivative of sway force with respect to yaw velocity | $\partial Y / \partial r$ | Ns |
| Y_R | YRU | Transverse rudder force | | N |
| $Y_{\dot{r}}$ | YRRT | Derivative of sway force with respect to yaw acceleration | $\partial Y / \partial \dot{r}$ | Ns ² |
| Y_v | YV | Derivative of sway force with respect to sway velocity | $\partial Y / \partial v$ | Ns/m |
| $Y_{\dot{v}}$ | YVRT | Derivative of sway force with respect to sway acceleration | $\partial Y / \partial \dot{v}$ | Ns ² /m |
| Y_{δ} | YD | Derivative of sway force with respect to rudder angle | $\partial Y / \partial \delta$ | N |
| Z | FZ | Heave force on body, force along body z -axis | | N |

2.4.1.5 Linear Models

| | | | | |
|------------|------|---|--|-------------------------------|
| C_r | CRDS | Directional stability criterion | $Y_v (N_r - \text{mux}_G) - N_v (Y_r - \text{mu})$ | N ² s ² |
| L_b, l_b | LSB | Static stability lever | N_v / Y_v | m |
| L_d, l_d | LSR | Damping stability lever | $(N_r - \text{mux}_G) / (Y_r - \text{mu})$ | m |
| T | TIC | Time constant of the 1 st order manoeuvring equation | | s |
| T_1 | TIC1 | First time constant of manoeuvring equation | | s |
| T_2 | TIC2 | Second time constant of manoeuvring equation | | s |
| T_3 | TIC3 | Third time constant of manoeuvring equation | | s |
| K | KS | Gain factor in linear manoeuvring equation | | 1/s |
| P_n | PN | P-number, heading change per unit rudder angle in one ship length | | 1 |

2.4.1.6 Turning Circles

| | | | | |
|--------------|--------|---|--|-------|
| D_C | DC | Steady turning diameter | | m |
| D_C' | DCNO | Non-dimensional steady turning diameter | D_C / L_{PP} | 1 |
| D_0 | DC0 | Inherent steady turning diameter $\delta_R = \delta_0$ | | m |
| D_0' | DC0N | Non-dimensional inherent steady turning diameter | D_0 / L_{PP} | 1 |
| l_r | LHRD | Loop height of r - δ curve for unstable ship | | rad/s |
| l_{δ} | LWRD | Loop width of r - δ curve for unstable ship | | rad |
| r_C | OZCI | Steady turning rate | | 1/s |
| r_C' | OZCINO | Non-dimensional steady turning rate | $r_C L_{PP} / U_C$ or $2 L_{PP} / D_C$ | m |
| R_C | RCS | Steady turning radius | | m |
| t_{90} | TI90 | Time to reach 90 degree change of heading | | s |
| t_{180} | TI180 | Time to reach 180 degree change of heading | | s |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|--|---------------------------|---------|
| U_C | UC | Speed in steady turn | | m/s |
| x_{090} | X090 | Advance at 90° change of heading | | m |
| x_{0180} | X0180 | Advance at 180° change of heading | | m |
| x_{0max} | XMx | Maximum advance | | m |
| y_{090} | Y090 | Transfer at 90° change of heading | | m |
| y_{0180} | Y0180 | Tactical diameter (transfer at 180° change of heading) | | m |
| y_{0max} | YOMx | Maximum transfer | | m |
| β_C | DRCI | Drift angle at steady turning | | rad |

2.4.1.7 Zig-Zag Manoeuvres

| | | | | |
|----------------|--------|-------------------------------------|--|-----|
| t_a | TIA | Initial turning time | | s |
| t_{c1} | TIC1 | First time to check yaw (starboard) | | s |
| t_{c2} | TIC2 | Second time to check yaw (port) | | s |
| t_{hc} | TCHC | Period of changes in heading | | s |
| t_r | TIR | Reach time | | s |
| y_{0max} | YOMx | Maximum transverse deviation | | m |
| δ_{max} | ANRUMx | Maximum value of rudder angle | | rad |
| ψ_s | PSIS | Switching value of course angle | | rad |
| ψ_{01} | PSI01 | First overshoot angle | | rad |
| ψ_{02} | PSI02 | Second overshoot angle | | rad |

2.4.1.8 Stopping Manoeuvres

| | | | | |
|----------|-----|-----------------------------------|--|---|
| s_F | SPF | Distance along track, track reach | | m |
| x_{0F} | X0F | Head reach | | m |
| y_{0F} | Y0F | Lateral deviation | | m |
| t_F | TIF | Stopping time | | s |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

2.4.2 Sea Keeping

Related information is to be found in Chapter 3 on General Mechanics in Sections 3.1.2 on Time and Frequency Domain Quantities, 3.1.3 on Stochastic Processes, 3.2.1 on Inertial Properties,, 3.2.2 on Loads, 3.2.3 on Rigid Body Motions, and 3.4.1 on Waves.

2.4.2.1 Basic Quantities

| | | | | |
|--|-----------------|--|--|------------------|
| A_{FS} | AFS | Projected area of stern fins | | m ² |
| a_i | AT(I) | Attitudes of the floating system | $i = 1, 2, 3$, e.g. Euler angles of roll, pitch, and yaw, respectively | rad |
| f | FR | Frequency | $1 / T$ | Hz |
| f_E | FE | Frequency of wave encounter | $1 / T_E$ | Hz |
| f_z | | Natural frequency of heave | $1 / T_z$ | Hz |
| f_θ | | Natural frequency of pitch | $1 / T_\theta$ | Hz |
| f_ϕ | | Natural frequency of roll | $1 / T_\phi$ | Hz |
| F_L | FS(2) | Wave excited lateral shear force | Alias horizontal! | N |
| F_N | FS(3) | Wave excited normal shear force | Alias vertical! | N |
| M_L | MB(3), FS(6) | Wave excited lateral bending moment | Alias horizontal! | Nm |
| M_N | MB(2), FS(5) | Wave excited normal bending moment | Alias vertical! | Nm |
| M_T | MT(1), FS(4) | Wave excited torsional moment | | Nm |
| n_{AW} | NAW | Mean increased rate of revolution in waves | | 1/s |
| P_{AW} | PAW | Mean power increased in waves | | W |
| Q_{AW} | QAW | Mean torque increased in waves | | Nm |
| R_{AW} | RAW | Mean resistance increased in waves | | N |
| $S_\eta(f)$, $S_{\eta\eta}(f)$, $S_\eta(\omega)$, $S_{\eta\eta}(\omega)$ | EWSF, EWSC | Wave elevation auto spectral density | see also section 1.4.1, Waves | m ² s |
| x_i | X(I) | Absolute displacement of the ship at the reference point | $i = 1, 2, 3$:surge, sway, and heave respectively | m |
| x_u | X(U) | Generalized displacement of a ship at the reference point | $u = 1...6$ surge, sway, heave, roll, pitch, yaw | m, rad |
| T_{AW} | TAW | Mean thrust increase in waves | | N |
| T | TC | Wave period | | s |
| T_e | TE | Wave encounter period | | s |
| T_z | TNHE | Natural period of heave | | s |
| T_θ | TNPI | Natural period of pitch | | s |
| T_ϕ | TNRO | Natural period of roll | | s |
| $Y_z(\omega)$, $A_{z\zeta}(\omega)$ | | Amplitude of frequency response function for translatory motions | $z_a(\omega) / \zeta_a(\omega)$ or $z_a(\omega) / \eta_a(\omega)$ | 1 |
| $Y_{\theta\zeta}(\omega)$, $A_{\theta\zeta}(\omega)$ | | Amplitude of frequency response function for rotary motions | $\Theta_a(\omega) / \zeta_a(\omega)$ or $\Theta_a(\omega) / (\omega^2 / (g\zeta_a(\omega)))$ | 1 |
| Λ | | Tuning factor | $\Lambda_z = \frac{\omega_E}{\omega_z}$ $\Lambda_\theta = \frac{\omega_E}{\omega_\theta}$ $\Lambda_\phi = \frac{\omega_E}{\omega_\phi}$ or $\Lambda_z = \frac{T_z}{T_E}$ $\Lambda_\theta = \frac{T_\theta}{T_E}$ $\Lambda_\phi = \frac{T_\phi}{T_E}$ | |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|----------------------|--|-------------|
| μ | | Wave encounter angle | Angle between ship positive x axis and positive direction of waves (long crested) or dominant wave direction (short crested) | rad |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

2.4.3 Large Amplitude Motions Capsizing

| | | | | |
|----------------------|------|---|--|----------------|
| A | | Assumed centre of gravity above keel used for cross curves of stability - I99/1.2.4.1 | | 1 |
| \overline{AB} | XAB | Longitudinal centre of buoyancy from aft perpendicular - I99/1.2.4.2 | Distance of centre of buoyancy from aft perpendicular | m |
| A_C | | Area of deck available to crew | | m ² |
| \overline{AF} | XAF | Distance of the centre of flotation from after perpendicular | | m |
| \overline{AG}_L | XAG | Longitudinal centre of gravity from aft perpendicular | Distance of centre of gravity from aft perpendicular | m |
| \overline{AG}_T | YAG | Transverse distance from assumed centre of gravity A, to actual centre of gravity G | | m |
| \overline{AG}_V | ZAG | Vertical distance from assumed centre of gravity A, to actual centre of gravity G | | m |
| A_{LV} | AHLV | Lateral area of hull above water | | m ² |
| A_{RL} | | Positive area under righting lever curve | | m ² |
| A_{SI} I_{AS} | ASI | Attained subdivision index | | 1 |
| A_S | AS | Area of sails in profile according to ISO 8666 | | m ² |
| A_v | AV | Projected lateral area of the portion of the ship and deck cargo above the waterline - IMO/IS, IMO/HSC'2000 | | m ² |
| \overline{AZ} | YAZ | Righting arm based on horizontal distance from assumed centre of gravity A, to Z | Generally tabulated in cross curves of stability | m |
| B | | Centre of buoyancy | Centroid of the underwater volume | |
| B_{CB} | | Beam between centres of buoyancy of side hulls | | m |
| \overline{BM} | ZBM | Transverse metacentre above centre of buoyancy | Distance from the centre of buoyancy CB to transverse metacentre M $\overline{BM} = \frac{I_T}{\nabla} = \overline{KM} - \overline{KB}$ | m |
| \overline{BM}_L | ZBML | Longitudinal metacentre above centre of buoyancy | $\overline{BM}_L = \overline{KM}_L - \overline{KB}$ | m |
| b | | Centre of flotation of added buoyancy layer or centre of lost buoyancy of the flooded volume | | |
| b | | Maximum tank breadth | | m |
| C_D | | Crew density | Proportion of boat plan needed for crew | |
| C_H | | Height coefficient, depending on the height above sea level of the structural member exposed to the wind | | 1 |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-----------------------|-----------------|--|---|---------|
| C_{Lcp} | | Crew limit | Maximum number of persons on board | |
| C_{MTL} | CMTL | Longitudinal trimming coefficient - I99/1.2.4.3 | Trimming moment divided by change in trim which approximately equals \overline{BM}_L / L | 1 |
| C_s | | Shape coefficient, depending on the shape of the structural member exposed to the wind | | 1 |
| d | T | Draught, moulded, of ship hull - I99/1.2.1 | | m |
| d | | Density coefficient for submerged test weights | | 1 |
| F | | Centre of flotation of the water plane | | |
| F | | Wind force - IMO/IS | | |
| f | FREB | Freeboard | From the freeboard markings to the freeboard deck, according to official rules | m |
| \overline{FB} | XFB | Longitudinal centre of buoyancy, L_{CB} , from forward perpendicular | Distance of centre of buoyancy from forward perpendicular | m |
| \overline{FF} | XFF | Longitudinal centre of flotation, L_{CF} , from forward perpendicular | Distance of centre of flotation from forward perpendicular | m |
| \overline{FG} | XFG | Longitudinal centre of gravity, from forward perpendicular | Distance of centre of gravity from forward perpendicular | m |
| G | | Centre of gravity of a vessel | | |
| g | | Centre of gravity of an added or removed weight (mass) | | 1 |
| \overline{GG}_1 | GGV | Vertical stability lever caused by a weight shift or weight addition | $\overline{KG}_1 = \overline{KG}_0 + \overline{GG}_1$ | m |
| \overline{GG}_H | GGH | Horizontal stability lever caused by a weight shift or weight addition | | m |
| \overline{GG}_L | GGL | Longitudinal stability lever caused by a weight shift or weight addition | | m |
| \overline{GG}_V | GGV | Vertical stability lever caused by a weight shift or weight addition | $\overline{KG}_1 = \overline{KG}_0 + \overline{GG}_1$ | m |
| \overline{GM} | GM | Transverse metacentric height | Distance of centre of gravity to the metacentre $\overline{GM} = \overline{KM} - \overline{KG}$ (not corrected for free surface effect) | m |
| \overline{GM}_{EFF} | GMEFF | Effective transverse metacentric height | \overline{GM} Corrected for free surface and/or free communication effects | m |
| \overline{GM}_L | GML | Longitudinal metacentric height | Distance from the centre of gravity G to the longitudinal metacentre M_L $\overline{GM}_L = \overline{KM}_L - \overline{KG}$ | m |
| \overline{GZ} | GZ | Righting arm or lever | $\overline{GZ} = \overline{AZ} - \overline{AG}_V \sin \varphi - \overline{AG}_T \cos \varphi$ | m |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-----------------------|-----------------|--|---|---------|
| \overline{GZ} | | Arm of static stability corrected for free surfaces - IMO/table | | m |
| \overline{GZ}_{MAX} | GZMAX | Maximum righting arm or lever | | m |
| h | | Maximum tank height | | m |
| h_{CE} | | Height of centre of area of A_{SP} above waterline at SSM | | m |
| HL | | Heeling lever (due to various reasons) - IMO/HSC'2000 | | m |
| h_{LP} | | Height of waterline above centre of area of immersed profile | | m |
| K | | Keel reference | | |
| \overline{KA} | ZKA | Assumed centre of gravity above moulded base of keel | Distance from the assumed centre of gravity A to the moulded base of keel or K | m |
| \overline{KB} | ZKB | Centre of buoyancy above moulded base of keel | Distance from the centre of buoyancy B to the moulded base of keel or K | m |
| \overline{KG} | ZKG | Centre of gravity above moulded base of keel | Distance from the centre of gravity G to the moulded base of keel or K | m |
| \overline{Kg} | ZKAG | Vertical centre of gravity of added or removed weight above moulded base of keel | Distance from the assumed centre of gravity, g , to the moulded base of keel or K | m |
| \overline{KM} | ZKM | Transverse metacentre above moulded base of keel | Distance from the transverse metacentre M to the moulded base of keel or K | m |
| \overline{KM}_L | ZKML | Longitudinal metacentre above moulded base of keel | Distance from the longitudinal metacentre M_L to the moulded base of keel or K | m |
| k | | Roll damping coefficient expressing the effect of bilge keels | | 1 |
| L | | Length of the vessel on the waterline in maximum load condition - IMO/IS | | m |
| l | | Arm of dynamic stability corrected for free surfaces - IMO/table | | m |
| l | XTA | Longitudinal trimming arm | $X_{CG} - X_{CB}$ | m |
| l | | Maximum tank length | | m |
| l_s | | Actual length of enclosed superstructure extending from side to side of the vessel | | m |
| l_w | | Wind heeling lever | | m |
| M | | Metacentre of a vessel | See subscripts for qualification | |
| m | SHIPMA | Ship mass | W/g | kg |
| M_C | | Maximum offset load moment due to crew | | Nm |
| M_c | | Minimum capsizing moment as determined when account is taken of rolling | | Nm |
| M_{FS} | | Free surface moment at any inclination | | Nm |
| m_{LCC} | | Mass in light craft condition | | kg |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|----------------------|-----------------|---|--|----------------|
| m_{LDC} | | Mass in loaded displacement condition according to ... | | kg |
| m_{MTL} | | Maximum total load (mass) | | kg |
| M_R | | Heeling moment due to turning | | Nm |
| M_S | MS | Moment of ship stability in general | $\Delta \overline{GZ}$. Other moments such as those of capsizing, heeling, etc. will be represented by M_S with additional subscripts as appropriate. | Nm |
| m_{SSC} | | Mass in standard sailing conditions according to ... | | kg |
| M_{TC} | MTC | Moment to change trim one centimetre | | Nm/cm |
| M_{TM} | MTM | Moment to change trim one meter | ΔC_{MTL} | Nm/m |
| M_W | | Maximum heeling moment due to wind | | Nm |
| M_v | | Dynamically applied heeling moment due to wind pressure | | Nm |
| \overline{OG} | | Height of centre of gravity above waterline | | m |
| P_V | | Wind pressure | | Pa |
| r | | Effective wave slope coefficient | | 1 |
| R_{SI} | RSI | Required subdivision index | | 1 |
| s | | Wave steepness | | 1 |
| $STIX$ | STIX | Actual stability index value according to ... | | 1 |
| \overline{STIX} | STIXR | Required stability index value, see ... | | 1 |
| T | YHA | Equivalent transverse heeling arm | Heeling moment/ Δ | m |
| TL | | Turning lever | | m |
| t_s t_{KL} | TRIM | Static trim | $T_A - T_F - d_{KL}$ | m |
| V v | | Tank total capacity | | m ³ |
| V_0 | | Speed of craft in the turn - IMO/HSC'2000 Service speed - IMO/IS | | m/s |
| v_W | | Wind speed used in calculation | | m/s |
| W | SHIPWT | Ship weight | $m g$ | N |
| x_{CB} | XACB | Longitudinal centre of floatation of added buoyant layer | Longitudinal distance from reference point to the centre of the added buoyant layer, b | m |
| X_{CB} L_{CB} | XCB | Longitudinal centre of buoyancy (L_{CB}) | Longitudinal distance from reference point to the centre of buoyancy, B | m |
| X_{CF} L_{CF} | XCF | Longitudinal centre of flotation (L_{CF}) | Longitudinal distance from reference point to the centre of flotation, F | m |
| x_{CG} | XACG | Longitudinal centre of gravity of added weight (mass) | Longitudinal distance from reference point to the centre of gravity, g, of an added or removed weight (mass) | m |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-----------------------|-----------------|--|--|----------------|
| X_{CG} L_{CG} | XCG | Longitudinal centre of gravity (L_{CG}) | Longitudinal distance from reference point to the centre of gravity, G | m |
| X_1, X_2 | | Roll damping coefficients | | 1 |
| x_D | | Distance of down flooding opening from end of boat | | m |
| $Y_{CG},$ y_{CG} | YCG | Lateral displacement of centre of gravity (Y_{CG}) | Lateral distance from a reference point to the centre of gravity, G | m |
| y_D | | Distance of down flooding opening from gunwale | | m |
| y_D' | | Distance of down flooding opening off centreline | | m |
| Z | ZRA | Intersection of righting arm with line of action of the centre of buoyancy | | |
| Z | | Vertical distance from the centre of A to the centre of the underwater lateral area or approximately to a point at one half the draught - IMO/IS | | m |
| Z, h | | Vertical distance from the centre of A to the waterline | | m |
| z_D | | Height above waterline of down flooding opening | | m |
| z_{SA} | ZSA | Static sinkage at AP | Caused by loading | m |
| z_{SF} | ZSF | Static sinkage at FP | Caused by loading | m |
| z_S | ZS | Mean static sinkage | $(z_{SF} + z_{SA})/2$ | m |
| δ | | Tank block coefficient | | 1 |
| δ_{KL} | DTR | Change in static trim | | m |
| Δ | DISPF | Displacement (buoyant) force | $g \rho \nabla$ | N |
| Δ_m | DISPM | Displacement mass | $\rho \nabla$ | kg |
| ∇ | DISPVOL | Displacement volume | $\Delta / (\rho g)$ | m ³ |
| ∇_{fw} | DISVOLFW | Displacement volume of flooded water | $\Delta_{fw} / (\rho g)$ | m ³ |
| ϕ | HEELANG | Heel angle | | rad |
| ϕ_0 | | Heel angle during offset load tests | | rad |
| $\phi_{0(REQ)}$ | | Maximum permitted heel angle during ... | | rad |
| ϕ_D | | Actual down flooding angle according to ... | | rad |
| $\phi_{D(REQ)}$ | | Required down flooding angle, see... | | rad |
| ϕ_{DC} | | Down flooding angle to non-quick draining cockpits | | rad |
| ϕ_{DH} | | Down flooding angle to any main access hatchway | | rad |
| ϕ_F | HEELANGF | Heel angle at flooding | | rad |
| ϕ_{GZMAX} | | Angle of heel at which maximum righting moment occurs | | rad |
| ϕ_R | | Assumed roll angle in a seaway | | rad |
| ϕ_{VS} | HEELANGV | Heel angle for vanishing stability | | rad |
| ϕ_W | | Heel angle due to calculation wind | | rad |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|---|---|-------------------|
| μ | PMVO | Volumetric permeability | The ratio of the volume of flooding water in a compartment to the total volume of the compartment | 1 |
| θ_c | | Capsizing angle under the action of a gust of wind IMO/IS | | rad |
| ϕ_m | | Heel angle corresponding to the maximum of the statical stability curve | | rad |
| θ_s | TRIMS | Static trim angle | $\tan^{-1}((z_{SF}-z_{SA})/L)$ | rad |
| ρ | RHO | (Liquid) mass density | | kg/m ³ |
| ρ_A | RHOA DNA | (Air) mass density | | kg/m ³ |
| ρ_S | DNWA | (Water) mass density | | kg/m ³ |

2.4.4 Symbols for Attributes and Subscripts

| | |
|-----------|----------|
| A | Aft |
| E | Entrance |
| F | Fore |
| R | Run |
| Z | Heave |
| θ | Pitch |
| φ | Roll |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

3. SPECIAL CRAFT

3.1 Planing and Semi-Displacement Vessels

3.1.1 Geometry and Hydrostatics

See also Section 1.2.1, Hull Geometry and Section 1.2.2 Propulsor Geometry

| | | | | |
|--------------------|-------|--|---|----------------|
| A_P | APB | Planing bottom area | Horizontally projected planing bottom area (at rest), excluding area of external spray strips | m ² |
| B_{LCG} | BLCG | Beam at longitudinal position of the centre of gravity | Breadth over spray strips measured at transverse section containing centre of gravity | m |
| B_{PC} | BPC | Beam over chines | Beam over chines, excluding external spray strips | m |
| B_{PA} | BPA | Mean breadth over chines | A_P / L_P | m |
| B_{PT} | BPT | Transom breadth | Breadth over chines at transom, excluding external spray strips | m |
| B_{PX} | BPX | Maximum breadth over chines | Maximum breadth over chines, excluding external spray strips | m |
| L_{SB} | LSB | Total length of shafts and bossings | | m |
| L_{PR} | LPRC | Projected chine length | Length of chine projected in a plane parallel to keel | m |
| β | BETD | Deadrise angle of planing bottom | Angle between a straight line approximating body section and the intersection between basis plane and section plane | rad |
| β_M | BETM | Deadrise angle at midship section | | rad |
| β_T | BETT | Deadrise angle at transom | | rad |
| ε_{SH} | EPSSH | Shaft angle | Angle between shaft line and reference line (positive, shaft inclined downwards) | rad |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

3.1.2 Geometry and Levers, Underway

3.1.2.1 Geometry, Underway

| | | | | |
|----------------------|---------|---|--|----------------|
| d_{TR} | DTRA | Immersion of transom, underway | Vertical depth of trailing edge of boat at keel below water surface level | m |
| h_P | HSP | Wetted height of strut palms (flange mounting) | | m |
| h_R | HRU | Wetted height of rudders | | m |
| L_C | LC | Wetted chine length, underway | | m |
| l_{CP} | LCP | Lever of resultant of pressure forces, underway | Distance between centre of pressure and aft end of planing surface | m |
| L_K | LK | Wetted keel length, underway | | m |
| L_M | LM | Mean wetted length, underway | $(L_K + L_C) / 2$ | m |
| S_{WHP} | SWHP | Wetted area underway of planing hull | Principal wetted area bounded by trailing edge, chines and spray root line | m ² |
| S_{WB} | SWB | Wetted bottom area, underway | Area bounded by stagnation line, chines or water surface underway and transom | m ² |
| S_{WHE} | SWHE | Wetted hull area, underway | Total wetted surface of hull underway, including spray area and wetted side area, w/o wetted transom area | m ² |
| S_{WHS} | SWSH | Area of wetted sides | Wetted area of the hull side above the chine or the design water line | m ² |
| S_{WS}, S_S | SWS | Area wetted by spray | Wetted area between design line or stagnation line and spray edge | m ² |
| α_B | ALFSL | Angle of stagnation line | Angle between projected keel and stagnation line in a in plane normal to centre plane and parallel to reference line | rad |
| α_{BAR} | ALFBAR | Barrel flow angle | Angle between barrel axis and assumed flow lines | rad |
| ϵ_{WL} | EPSWL | Wetted length factor | L_M / L_{WL} | 1 |
| ϵ_{WS} | EPSWS | Wetted surface area factor | S / S_0 | 1 |
| θ_{DWL} | TRIMDWL | Running trim angle based on design waterline | Angle between design waterline and running waterline (positive bow up) | rad |
| θ_S, θ_0 | TRIMS | Static trim angle | Angle between ship design waterline and actual water line at rest (positive bow up) $\tan^{-1}((z_{SF} - z_{SA}) / L)$ | rad |
| θ_V, θ_D | TRIMV | Running (dynamic) trim angle | Angle between actual water line at rest and running water line (positive bow up) $\tan^{-1}((z_{VF} - z_{VA}) / L)$ | rad |
| λ_W | LAMS | Mean wetted length-beam ratio | $L_M / (B_{LCG})$ | 1 |
| τ | TRIMDWL | Running trim angle based on design waterline | Angle between design waterline and running waterline (positive bow up) | deg |
| τ_{DWL} | TAUDWL | Reference line angle | Angle between the reference line and the design waterline | rad |
| τ_R | TAUR | Angle of attack relative to the reference line | Angle between the reference line and the running waterline | rad |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|------------------|-----------------|---|---|---------|
| ϕ_{SP} | PHISP | Spray angle | Angle between stagnation line and keel (measured in plane of bottom) | rad |
| δ_λ | DLAM | Dimensionless increase in total friction area | Effective increase in friction area length-beam ratio due to spray contribution to drag | 1 |

3.1.2.2 Levers, Underway

| | | | | |
|----------|-------|--|--|---|
| e_A | ENAPP | Lever of appendage lift force N_A | Distance between N_A and centre of gravity (measured normally to N_A) | m |
| e_B | ENBOT | Lever of bottom normal force N_B | Distance between N_B and centre of gravity (measured normally to N_B) | m |
| e_{PN} | ENPN | Lever of propeller normal force N_{PN} | Distance between propeller centre-line and centre of gravity (measured along shaft line) | m |
| e_{PP} | ENPP | Lever of resultant of propeller pressure forces N_{PP} | Distance between N_{PP} and centre of gravity (measured normally to N_{PP}) | m |
| e_{PS} | ENPS | Lever of resultant propeller suction forces N_{PS} | Distance between N_{PS} and centre of gravity (measured normal to N_{PS}) | m |
| e_{RP} | ENRP | Lever of resultant of rudder pressure forces N_{RP} | Distance between N_{RP} and centre of gravity (measured normal to N_{RP}) | m |
| f_{AA} | FRAA | Lever of wind resistance R_{AA} | Distance between R_{AA} and centre of gravity (measured normal to R_{AA}) | m |
| f_{AP} | FRAP | Lever of appendage drag R_{AP} | Distance between R_{AP} and centre of gravity (measured normal to R_{AP}) | m |
| f_F | FRF | Lever of frictional resistance R_F | Distance between R_F and centre of gravity (measured normal to R_F) | m |
| f_K | FRK | Lever of skeg or keel resistance R_K | Distance between R_K and centre of gravity (measured normal to R_K) | m |
| f_R | FDRR | Lever of augmented rudder drag ΔR_{RP} | Distance between ΔR_{RP} and centre of gravity (measured normal to ΔR_{RP}) | m |
| f_S | FSL | Lever of axial propeller thrust | Distance between axial thrust and centre of gravity (measured normal to shaft line) | m |
| f_T | FRT | Lever of total resistance R_T | Distance between R_T and centre of gravity (measured normal to R_T) | m |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

3.1.3 Resistance and Propulsion

See also Sections 2.3.1 on Hull Resistance

| | | | | |
|--------------|-------|---|--|-----|
| C_{L0} | CL0D | Lift coefficient for zero deadrise | $\Delta / (B_{CG}^2 q)$ | 1 |
| $C_{L\beta}$ | CLBET | Lift coefficient for deadrise surface | $\Delta / (B_{CG}^2 q)$ | 1 |
| C_V | CSP | Froude number based on breadth | $V / (B_{CG} g)^{1/2}$ | 1 |
| C_A | CDL | Load coefficient | $\Delta / (B_{CG}^3 \rho g)$ | 1 |
| L_{VHD} | LVD | Vertical component of hydrodynamic lift | | N |
| L_{VS} | LVS | Hydrostatic lift | Due to buoyancy | N |
| F_{TA} | FTAPP | Appendage drag force (parallel to reference line) | Drag forces arising from appendages inclined to flow, assumed to act parallel to the reference line | N |
| F_{TB} | FTBOT | Bottom frictional force (parallel to reference line) | Viscous component of bottom drag forces assumed acting parallel to the reference line | N |
| F_{TK} | FTKL | Keel or skeg drag force (parallel to reference line) | Drag forces arising from keel or skeg, assumed to act parallel to the reference line | N |
| F_{TRP} | FTRP | Additional rudder drag force (parallel to reference line) | Drag forces arising from influence of propeller wake on the rudder assumed to act parallel to the reference line | N |
| N_A | NAPP | Appendage lift force (normal to reference line) | Lift forces arising from appendages inclined to flow, assumed to act normally to reference line | N |
| N_B | NBOT | Bottom normal force (normal to reference line) | Resultant of pressure and buoyant forces assumed acting normally to the reference line | N |
| N_{PP} | NPP | Propeller pressure force (normal to reference line) | Resultant of propeller pressure forces acting normally to the reference line | N |
| N_{PS} | NPS | Propeller suction force (normal to reference line) | Resultant of propeller suction forces acting normally to the reference line | N |
| N_{RP} | NRP | Rudder pressure force (normal to reference line) | Resultant of rudder pressure forces acting normally to the reference line | N |
| R_K | RKEEL | Keel drag | | N |
| R_π | RPI | Induced drag | $g \rho V \tan \tau$ | N |
| R_{PAR} | RPAR | Parasitic drag | Drag due to inlet and outlet openings | N |
| R_{PS} | RSP | Pressure component of spray drag | | N |
| R_T | RT | Total resistance | Total towed resistance | N |
| R_{VS} | RSV | Viscous component of spray drag | $C_F S_{ws} q_s$ | N |
| V_{BM} | VBM | Mean bottom velocity | Mean velocity over bottom of the hull | m/s |
| V_{SP} | VSP | Spray velocity | Relative velocity between hull and spray in direction of the spray | m/s |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

3.2 Multi-Hull Vessels (Add trimaran symbols)

3.2.1 Geometry and Hydrostatics

See also Section 2.2.1, Hull Geometry

| | | | | |
|----------|--------|--|---|----------------|
| A_I | AIA | Strut-hull intersection area | | m ² |
| B_B | BB | Box beam | Beam of main deck | m |
| B_S | BS | Hull spacing | Distance between hull centre lines | m |
| B_{TV} | BTUN | Tunnel width | Minimal distance of the demihulls at the waterline | m |
| D_H | DHUL | Hull diameter | Diameter of axis symmetric submerged hulls | m |
| D_X | DX | Hull diameter at the longitudinal position "X" | | m |
| H_{DK} | HCLDK | Deck clearance | Minimum clearance of wet deck from water surface at rest | m |
| H_{SS} | HSS | Strut submerged depth | Depth of strut from still water line to strut-hull intersection | m |
| i_{EI} | ANENIN | Half angle of entrance at tunnel (inner) side | Angle of inner water line with reference to centre line of demihull | rad |
| i_{EO} | ANENOU | Half angle of entrance at outer side | Angle of outer water line with reference to centre line of demihull | rad |
| L_{CH} | LCH | Length of centre section of hull | Length of prismatic part of hull | m |
| L_{CS} | LCS | Length of centre section of strut | Length of prismatic part of strut | m |
| L_H | LH | Box length | Length of main deck | m |
| L_{NH} | LNH | Length of nose section of hull | Length of nose section of hull with variable diameter | m |
| L_{NS} | LNS | Length of nose section of strut | Length of nose section of strut with variable thickness | m |
| L_S | LS | Strut length | Length of strut from leading to trailing edge | m |
| L_{SH} | LSH | Length of submerged hull | | m |
| t_S | TSTR | Maximum thickness of strut | | m |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

3.2.2 Resistance and Propulsion

3.2.2.1 Resistance Components

See also Section 2.3.1 on Hull Resistance

| | | | | |
|------------|-------|---|------------------------|---|
| R_{FMH} | RFMH | Frictional resistance of multi-hull vessel | | N |
| R_{FINT} | RFINT | Frictional resistance interference correction | $R_{FMH} - \Sigma R_F$ | N |
| R_{RMH} | RRMH | Residuary resistance correction of multi-hull | $R_{TMH} - R_{FMH}$ | N |
| R_{RI} | RRINT | Residuary resistance interference correction | $R_{RMH} - \Sigma R_R$ | N |
| R_{TMH} | RTMH | Total resistance of multi-hull vessel | | N |
| R_{TI} | RTINT | Total resistance interference correction | $R_{TMH} - \Sigma R_T$ | N |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

3.3 Hydrofoil Boats

3.3.1 Geometry and Hydrostatics

See Sections 2.2.1 and 2.2.4

| | | | | |
|---------------|-------|---|-------------------------------|----------------|
| A_F | AFO | Foil area (general) | Foil area in horizontal plane | m ² |
| A_{FT} | AFT | Total foil plane area | | m ² |
| B_{FOA} | BFOA | Maximum vessel breadth including foils | | m |
| b_S | BST | Span of struts | | m |
| b_{ST} | BSTT | Transverse horizontal distance of struts | | m |
| c_C | CHC | Chord length at centre plane | | m |
| c_F | CFL | Chord length of flap | | m |
| c_M | CHM | Mean chord length | | m |
| c_S | CSTR | Chord length of a strut | | m |
| c_{SF} | CHSF | Chord length of strut at intersection with foil | | m |
| c_T | CHTI | Chord length at foil tips | | m |
| W_F | WTF | Weight of foil | | N |
| α_c | ALFTW | Geometric angle of twist | | rad |
| θ_{DH} | DIHED | Dihedral angle | | rad |
| V_F | DISVF | Foil displacement volume | | m ³ |

3.3.1.1 Geometry, Underway

| | | | | |
|------------|-------|--|---|----------------|
| A_{FE} | AFE | Emerged area of foil | | m ² |
| A_{FF} | ASFF | Submerged area of front foil | | m ² |
| A_{FR} | ASFR | Submerged area of rear foil | | m ² |
| A_{FS} | AFS | Submerged foil area | | m ² |
| A_{FST0} | AFSTO | Submerged foil plan area at take-off speed | | m ² |
| A_{SS} | ASS | Submerged strut area | | m ² |
| b_w | BSPW | Foil span wetted | | m |
| c_{PF} | CPFL | Distance of centre of pressure on a foil or flap from leading edge | | m |
| Fr_L | FNFD | Froude number based on foil distance | $V / (g L_F)^{1/2}$ | 1 |
| Fr_c | FNC | Froude number based on chord length | $V / (g c_M)^{1/2}$ | 1 |
| h_{CG} | HVCG | Height of centre of gravity foilborne | Distance of centre of gravity above mean water surface | m |
| h_F | HFL | Flight height | Height of foil chord at foilborne mode above position at rest | m |
| h_K | HKE | Keel clearance | Distance between keel and mean water surface foilborne | m |
| l_F | LEFF | Horizontal distance of centre of pressure of front foil to centre of gravity | | m |
| l_{FR} | LEFR | Horizontal distance between centres of pressure of front and rear foils | $l_F + l_R$ | m |
| l_R | LERF | Horizontal distance of centre of pressure of rear foil to centre of gravity | | m |
| T_F | TFO | Foil immersion | Distance between foil chord and mean water surface | m |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|---|---|-------------|
| T_{FD} | TFD | Depth of submergence of apex of a dihedral foil | Distance between foil apex and mean water surface | m |
| T_{FM} | TFOM | Mean depth of foil submergence | | m |
| α_{IND} | ALFIND | Downwash or induced angle | | rad |
| α_M | ALFM | Angle of attack of mean lift coefficient for foils with twist | | rad |
| α_s | AFS | Angle of attack for which flow separation (stall) occurs | | rad |
| α_{TO} | ATO | Incidence angle at take-off speed | | rad |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

3.3.2 Resistance and Propulsion

See also Section 2.3.1 Hull Resistance

3.3.2.1 Basic Quantities

| | | | | |
|-----------|-------|---|--|----|
| D_F | DRF | Foil drag | Force in the direction of motion of an immersed foil | N |
| D_{FR} | DFA | Drag force on rear foil | $C_{DF} A_{FR} q$ | N |
| D_{FF} | DFE | Drag force on front foil | $C_{DF} A_{FF} q$ | N |
| D_I | DRIND | Induced drag | For finite span foil, the component of lift in the direction of motion | N |
| D_{INT} | DRINT | Interference drag | Due to mutual interaction of the boundary layers of intersecting foil | N |
| D_{P0} | DRF0 | Profile drag for angle of attack equal to zero lift | Streamline drag | N |
| D_S | DRSP | Spray drag | Due to spray generation | N |
| D_{ST} | DRST | Strut drag | | N |
| D_W | DRWA | Wave drag | Due to propagation of surface waves | N |
| D_V | DRVNT | Ventilation drag | Due to reduced pressure at the rear side of the strut base | N |
| L_F | LF | Lift force on foil | $C_L A_{FT} q$ | N |
| L_{FF} | LFF | Lift force on front foil | $C_L A_{FF} q$ | N |
| L_{FR} | LFR | Lift force on rear foil | $C_L A_{FR} q$ | N |
| L_0 | LF0 | Profile lift force for angle of attack of zero | $C_{L0} A_{FT} q$ | N |
| L_{TO} | LT0 | Lift force at take off | $C_{LTO} A_{FT} q$ | N |
| M | MSP | Vessel pitching moment | | Nm |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

3.3.2.2 Derived Quantities

| | | | | |
|-----------------|--------|--|---|---|
| C_{DF} | CDF | Drag coefficient of foil | $D_F / (A_{FS} q)$ | 1 |
| C_{DI} | CDI | Induced drag coefficient | $D_I / (A_{FS} q)$ | 1 |
| C_{DINT} | CDINT | Interference drag coefficient | $D_{INT} / (A_{FS} q)$ | 1 |
| C_{D0} | CDO | Section drag coefficient for angle of attack equal to zero | $D_P / (A_{FS} q)$ | 1 |
| C_{DS} | CDSP | Spray drag coefficient | $D_S / (A_{FS} q)$ | 1 |
| C_{DVENT} | CDVENT | Ventilation drag coefficient | $D_V / (A_{FS} q)$ | 1 |
| C_{DW} | CDW | Wave drag coefficient | $D_W / (A_{FS} q)$ | 1 |
| C_{LF} | CLF | Foil lift coefficient | $L_F / (A_{FS} q)$ | 1 |
| C_{L0} | CLO | Profile lift coefficient for angle of attack equal to zero | $L_0 / (A_{FS} q)$ | 1 |
| C_{LTO} | CLTO | Lift coefficient at take-off condition | $L_{TO} / (A_{FS} q)$ | 1 |
| C_{LX} | CLA | Slope of lift curve | $dC_L / d\alpha$ | 1 |
| C_M | CM | Pitching moment coefficient | $M / ((A_{FF} + A_{FR}) (l_F - l_R) q)$ | 1 |
| M_F | MLF | Load factor of front foil | L_{FF} / Δ | 1 |
| M_R | MLR | Load factor of rear foil | L_{FR} / Δ | 1 |
| ε_F | EPSLDF | Lift/ Drag ratio of foil | L / D | 1 |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

3.4 ACV and SES

3.4.1 Geometry and Hydrostatics

See also [Section 1.2.1](#)

| | | | | |
|--------------------|--------|---|--|-------------------|
| A_C | CUA | Cushion area | Projected area of ACV or SES cushion on water surface | m ² |
| B_C | BCU | Cushion beam | SES cushion beam measured between the side walls | m |
| B_{WLT} | BWLT | Total waterline breadth of SES | At the water line | m |
| H_{CG} | HVCG | Height of centre of gravity above mean water plane beneath craft | | m |
| h_{BS} | HBS | Bow seal height | Distance from side wall keel to lower edge of bow seal | m |
| H_{SK} | HSK | Skirt depth | | m |
| h_{SS} | HSS | Stern seal height | Distance from side wall keel to lower edge of stern seal | m |
| L_B | LB | Deformed bag contact length | | m |
| L_C | LAC | Cushion length | | m |
| L_E | LACE | Effective length of cushion | A_C / B_C | m |
| S_{H0} | SSH0 | Wetted area of side hulls at rest off cushion | Total wetted area of side walls under way on cushion | m ² |
| S_{SHC} | SSHC | Wetted area of side hulls under way on cushion | Total wetted area of side walls under way on cushion | m ² |
| S_{SH} | SSH | Wetted area of side hulls under way off cushion | Total wetted area of side walls under way off cushion | m ² |
| X_H, L_H | XH, LH | Horizontal spacing between inner and outer side skirt hinges or attachment points to structure | needs clarification | m |
| X_S, L_S | XS, LS | Distance of leading skirt contact point out-board or outer hinge of attachment point to structure | needs clarification | m |
| Z_H, H_H | ZH, HH | Vertical spacing between inner and outer side skirt hinges or attachment points to structure | needs clarification | m |
| δB_C | DBCV | Increase in cushion beam due to water contact | | m |
| ε_{WS} | EPSWS | Wetted surface factor | S_{SHC} / S_{SH0} | 1 |
| θ_B | TETB | Bag contact deformation angle | | rad |
| θ_F | TETF | Finger outer face angle | | rad |
| θ_W | TETW | Slope of mean water plane for surface level beneath cushion periphery | | rad |
| ρ_A | DNA | (ACV and SES) Mass density of air | Mass of air per unit volume | kg/m ³ |
| ζ_C | ZETAC | Height of cushion generated wave above mean water plane at leading edge side of the skirt | | m |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

3.4.2 Resistance and Propulsion

See also Section 2.3.1 on Hull Resistance

| | | | | |
|-----------|-------|---------------------------------------|---------------------------------|-------------------|
| C_A | CLOAD | Cushion loading coefficient | $\Delta / (g \rho_A A_C^{3/2})$ | 1 |
| C_{PR} | CPR | Aerodynamic profile drag coefficient | $R_0 / (\rho_A V_R^2 A_C / 2)$ | 1 |
| C_{WC} | CWC | Cushion wave making coefficient | | 1 |
| p_B | PBM | Mean bag pressure | | Pa |
| p_{BS} | PBS | Bow seal pressure | Pressure in the bow seal bag | Pa |
| p_{CE} | PCE | Mean effective skirt pressure | | Pa |
| p_{CU} | PCU | Cushion pressure | Mean pressure in the cushion | Pa |
| p_{FT} | PFT | Fan total pressure | | Pa |
| p_{LR} | PLR | Cushion pressure to length ratio | P_{CU} / L_C | Pa/m |
| p_{SK} | PSK | Skirt pressure in general | | Pa |
| p_{SS} | PSS | Stern seal pressure | Pressure in the stern seal bag | Pa |
| P_{FCU} | PFCU | Power of lift fan | | W |
| P_{FSK} | PFSK | Power of skirt fan | | W |
| Q_{BS} | QBS | Bow seal air flow rate | Air flow rate to the bow seal | m ³ /s |
| Q_{CU} | QCU | Cushion air flow rate | Air flow rate to cushion | m ³ /s |
| Q_{SS} | QSS | Stern seal air flow rate | Air flow rate to the stern seal | m ³ /s |
| Q_T | QT | Total air volume flow | | m ³ /s |
| Q_{TS} | QTS | Total air volume flow of skirt | | m ³ /s |
| R_{AT} | RAT | Total aerodynamic resistance | $R_M + R_0$ | N |
| R_H | RH | Hydrodynamic resistance | $R_W + R_{WET}$ | N |
| R_M | RM | Intake momentum resistance in general | $\rho_A Q_T V_A$ | N |
| R_{MCU} | RMCU | Intake momentum resistance of cushion | $\rho_A Q_{CU} V_A$ | N |
| R_{ASK} | RASK | Intake momentum resistance of skirt | $\rho_A Q_{TS} V_A$ | N |
| R_{WET} | RWET | Resistance due to wetting | | N |
| T_C | TC0 | Cushion thrust | | N |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI-Unit |
|-------------|-----------------|------|---------------------------|---------|
|-------------|-----------------|------|---------------------------|---------|

3.5 Ice Going Vessels

3.5.1 Resistance and Propulsion

(See Figure 3.4, p 225 and Figure 3.8, p 231 of Vol. 1 of the *Proceedings of the 21st ITTC*)

| | | | | |
|----------------------------------|----------------------|---|--|-------------|
| C_I | CI | Coefficient of net ice resistance | $R_I / (\rho_I g h^2 B)$ | 1 |
| C_{IW} | CIW | Coefficient of water resistance in the presence of ice | $R_{IW} / (S q_{IW})$ | 1 |
| F_{IN} | FNIC | Normal ice force on a body | Projection of hull - ice interaction force on the external normal | N |
| F_{IT} | FTIC | Tangential ice force on a body | Projection of the hull - ice interaction force on the direction of motion | N |
| F_{rI} | FNIC | Froude number based on ice thickness | $V / (g h)^{1/2}$ | 1 |
| F_{XI} F_{YI} F_{ZI} | FXIC FYIC FZIC | Components of the local ice force | | N N N |
| f_{ID} | CFRD | Coefficient of friction between surface of body and ice (dynamic) | Ratio of tangential force to normal force between two bodies (dynamic condition) | 1 |
| f_{IS} | CFRS | Coefficient of friction between surface of body and ice (static) | The same as above (static condition) | 1 |
| h_I | HTIC | Thickness of ice | | m |
| h_{SN} | HTSN | Thickness of snow cover | | m |
| K_{QIA} | KQICMS | Average coefficient of torque in ice | $Q_{IA} / (\rho_W n_{IA}^2 D^5)$ | 1 |
| K_{TIA} | KTICMS | Average coefficient of thrust in ice | $T_{IA} / (\rho_W n_{IA}^2 D^4)$ | 1 |
| n_{IA} | FRICMS | Average rate of propeller revolution in ice | | Hz |
| P_{DI} | PDI | Delivered power at propeller in ice | $2 \pi Q_{IA} n_{IA}$ | W |
| Q_{IA} | QIMS | Average torque in ice | | Nm |
| R_I | RI | Net ice resistance | $R_{IT} - R_{IW}$ | N |
| R_{IT} | RIT | Total resistance in ice | Ship towing resistance in ice | N |
| R_{IW} | RIW | Hydrodynamic resistance in presence of ice | Total water resistance of ship in ice | N |
| T_{IA} | TIMS | Average total thrust in ice | | N |
| η_{ICE} | ERIC | Relative propulsive efficiency in ice | η_{ID} / η_D | 1 |
| η_{ID} | EFDIC | Propulsive efficiency in ice | $R_{IT} V / (2 \pi n_{IA} Q_{IA})$ | 1 |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

3.6 Sailing Vessels

3.6.1 Geometry and Hydrostatics

See also Section 2.2.1 on Hull Geometry

| | | | | |
|-----------------|-----------|--|--------------------------|----------------|
| A_J | ASJ | Area of jib or genoa | | m ² |
| A_{LK} | ALK | Lateral area of keel | | m ² |
| A_{LT} | ALT | Total lateral area of yacht | | m ² |
| A_m | ASM | Area of mainsail | | m ² |
| A_N | ASN | Normalized sail area | | m ² |
| A_{SP} | ASSP | Area of spinnaker | | m ² |
| A_S, S_A | AS | Sail area in general | $(P E + I J) / 2$ | m ² |
| B_{OA} | BOA | Beam, overall | | m |
| C_{pi} E | CPI EM | Center of pressure for A_i Main-sail base | | m |
| I | I | Fore triangle height | | m |
| J | J | Fore triangle base | | m |
| P | P | Mainsail height | | m |
| L_{EFF} | LEFF | Effective length for Reynolds Number | | m |
| S_C | SC | Wetted surface area of canoe body | | m ² |
| S_K | SK | Wetted surface area of keel | | m ² |
| S_R | SR | Wetted surface area of rudder | | m ² |
| T_C | TCAN | Draught of canoe body | | m |
| T_{EFF} | TEFF | Effective draught | $F_H / (\rho V_B^2 R)^5$ | m |
| Z_{CE} | ZCE | Height of centre of effort of sails above waterline in vertical centre plane | | m |
| V_C | DVCAN | Displaced volume of canoe body | | m ³ |
| V_K | DVK | Displaced volume of keel | | m ³ |
| V_R | DVR | Displaced volume of rudder | | m ³ |
| Δ_C | DFCAN | Displacement force (weight) of canoe body | | N |
| Δ_K | DFK | Displacement force (weight) of keel | | N |
| Δ_R | DFR | Displacement force (weight) of rudder | | N |

| ITTC Symbol | Computer Symbol | Name | Definition or Explanation | SI- Unit |
|----------------|--------------------|------|------------------------------|-------------|
|----------------|--------------------|------|------------------------------|-------------|

3.6.2 Resistance and Propulsion

| | | | | |
|-----------------|-------|---|---------------------|-----|
| C_{FU} | CFU | Frictional resistance coefficient (upright) | $R_{FU} / (S q)$ | 1 |
| C_{RU} | CRU | Residuary resistance coefficient (upright) | $R_{RU} / (S q)$ | 1 |
| C_{TU} | CTU | Total resistance coefficient (upright) | $R_{TU} / (S q)$ | 1 |
| C_{WU} | CWU | Wave resistance coefficient (upright) | | 1 |
| $C_{T\phi}$ | CTPHI | Total resistance coefficient with heel and leeway | $R_{T\phi} / (S q)$ | 1 |
| C_I | | Induced resistance coefficient | | 1 |
| C_x, C_y, C_z | | Force coefficients | | 1 |
| F_H | | Heeling force of sails | | N |
| F_R | | Driving force of sails | | N |
| F_V | | Vertical force of sails | | N |
| H | | Side force | | N |
| L_{HY} | | Hydrodynamic lift force | | N |
| R_{AW} | | Mean added resistance in waves | | N |
| R_{FU} | | Friction resistance (upright) | | N |
| R_{RU} | | Residuary resistance (upright) | | N |
| R_I | | Resistance increase due to side (induced resistance) | | N |
| R_{TU} | RTU | Total resistance (upright) | | N |
| $R_{T\phi}$ | RTUH | Total resistance when heeled | $R_{TU} + R_{\phi}$ | N |
| R_{ϕ}, R_H | RTUHA | Resistance increase due to heel (with zero side force) | | N |
| X, Y, Z | | Components of resultant force along designated axis | | N |
| V | V | Vessel velocity | | m/s |
| V_{WR} | VWR | Apparent wind velocity | | m/s |
| V_{WT} | VWT | True wind velocity | | m/s |
| V_{mc} | VMC | Velocity made good on course | | m/s |
| V_{mg} | VMG | Velocity made good to windward (contrary to wind direction) | | m/s |
| β_L | BETAL | leeway angle | | rad |
| β_{aw} | BETWA | apparent wind angle (relative to boat course) | | rad |
| β_{tw} | BETWT | true wind angle (relative to boat course) | | rad |

4. BACKGROUND AND REFERENCES

4.1 Symbols and Terminology Group

The tasks of the former Symbols and Terminology Group (SaT) have been handed over to the Quality Systems Group in 2002.

4.2 Description of the List of Symbols

4.2.1 Classification

The prime concern of the QS Group was to revise and try to complement the list of ITTC Standard Symbols sticking to the system for the classification of concepts.

With this regard, the following design requirements and goals have been maintained:

1. a coherent document, meeting the present and possibly the future requirements of the ITTC community in general and particular user groups
2. an open ended matrix structure that can be easily expanded as requirements arise, without the need of restructuring and repetition or too many explicit cross-references
3. minimized departures from the well established and widely accepted previous list of symbols

On the other hand, to facilitate the practical use of the list, a second version in which the symbols are arranged in alphabetic order was prepared. Symbols which have been listed several times in the matrix structured document have been maintained and for each symbol the field in which it is used is given in italic letters prior to the meaning of the symbol.

4.2.2 Structure of the Lists

The concepts related to a given subject area or model are designated by the ITTC Symbol and called by their Name. Their meaning can in principle only be concluded from the context of the model. The logically consistent, so called 'implicit' definition is derived from a definitely defined statement of the model, ideally a generally accepted system or an equivalent, e.g. a drawing.

The problem is that traditionally in lists of symbols, as in dictionaries, these explicit models are missing for various reasons. One reason is that many subject areas under discussion are

far from being developed and understood to the extent necessary. A consequence of this situation is that the symbols proposed are not always as coherent as would be necessary for advanced and systematic work, for which explicit models and adequate notations are essential.

The problem under discussion is of course the same in national and international standards. However there is an accepted international standard which deals with the general principles concerning physical quantities, equations, quantity and unit symbols, and coherent unit systems for general use within the various fields of science and technology (ISO 31).

4.2.3 Organization of the matrix structured list

As has been emphasized the development of symbols is a continuing process and as the subject develops, further amendments and additions, as approved by the Conference, will be included in future editions of the list.

In order to avoid any extra problems the symbols are arranged in alphabetical order in each subject area as in previous lists. Continuous page numbering was discarded in earlier versions. The idea was to establish a loose leaf organization as the most appropriate, in view of new draughts to be incorporated.

In view of the tremendous effort which explicit mathematical models, explanations, and sketches take for their preparation, the present QS Group can only follow the former SaT Group and state that the Technical Committees and other interested parties are urged to provide further material for review by the QS Group and future inclusion into the list.

It has been noted that some users dislike the disruption of the list of symbols by lengthy explanations. The present QS Group feels that the subject and the sensible use of the symbols require such explanations, also as the fundamentals of the theory of science and terminology often are not taught to students of naval architecture and marine engineering. However the arrangement has been changed so that these explanations can be visited by using hyperlinks and the list is not disrupted any more.

5. PRINCIPLES OF NOTATION

In Fig 1 the principles of notation in according to ISO 31 are shown.

Symbols representing physical quantities normally are one Latin or Greek letter with Subscripts for further identification. They are written in *italic* style letters.

Numbers are normally written in **roman** style letters. For more details, look at the list below or in the Excerpts of ISO 31 below or in standard itself.

Superscripts signify **operators** e.g.

- exponentiation
- the various aspects of complex quantities
- the various aspects of spectra and
- the various aspects of random quantities and stochastic processes e.g. probability operators.

Subscripts signify **identifiers**

- matrix components,
- identifiers tested, e.g. ship S or model M, appendages (App) or the various bodies in a multi-body problem,
- identifiers of coordinate systems and of the reference points, quantities(L_{PP})

| | | |
|------------------------------------|---|-----------------------------|
| Symbols for physical units | italic, one letter, except dimensionless quantities | A (e.g. Area in m^2) |
| Symbols for characteristic numbers | 2 letters italic | Re, Fr |
| Numbers | roman, generally | 10^3 |
| Symbols representing numbers | italic | x_{ij} |
| Units | roman, lower case unless derived from name | m, Pa |
| Prefix of units | roman | μm |
| Symbols for chemical elements | roman | H_2O |
| Symbols for universal constants | italic | $g = 9,80665 \text{ m/s}^2$ |

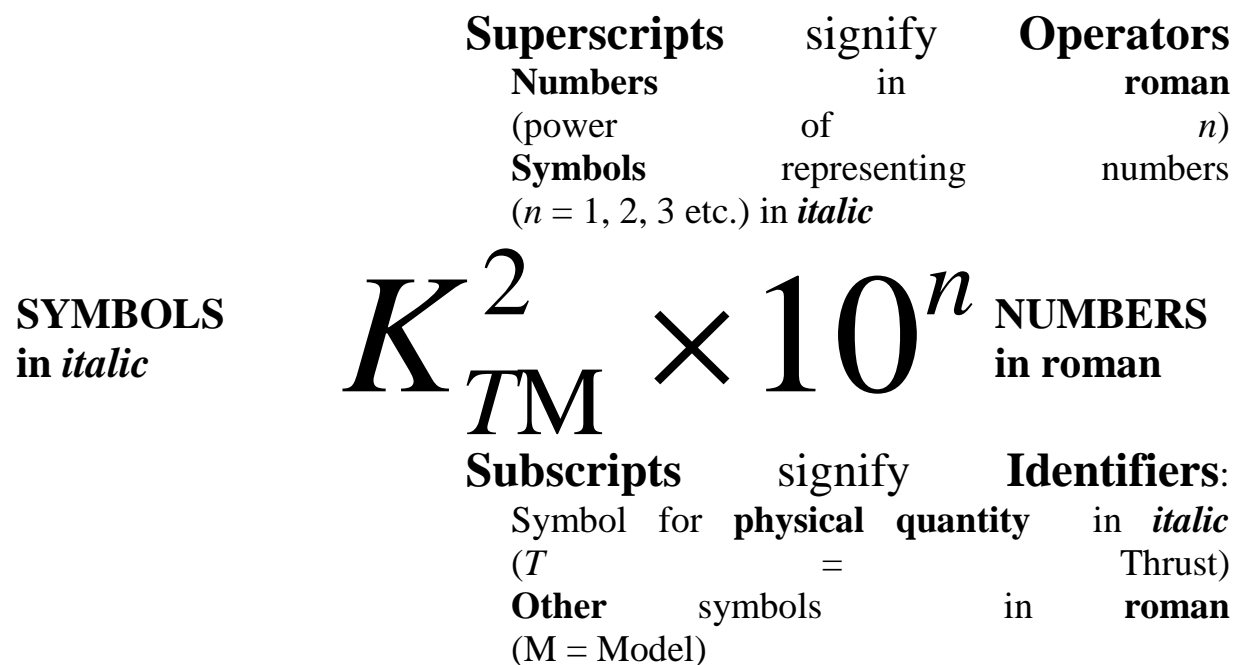


Fig. 1

5.1 Excerpts of ISO 31

1 Scope

This part of ISO 31 gives general information about principles concerning physical quantities, equations, quantity and unit symbols, and coherent unit systems, especially the International System of Units, SI.

The principles laid down in this part of ISO 31 are intended for general use within the various fields of science and technology and as a general introduction to the other parts of ISO 31.

2. Quantities and units

2.1 Physical quantity, unit and numerical value

In ISO 31 only physical quantities used for the quantitative description of physical phenomena are treated. Conventional scales, such as the Beaufort scale, Richter scale and colour intensity scales, and quantities expressed as the results of conventional tests, e.g. corrosion resistance, are not treated here, neither are currencies nor information contents.

Physical quantities may be grouped together into categories of quantities which are mutually comparable. Lengths, diameters, distances, heights, wavelengths and

so on would constitute such a category. Mutually comparable quantities are called "quantities of the same kind".

If a particular example of a quantity from such a category is chosen as a reference quantity, called the *unit*, then any other quantity from this category can be expressed in terms of this unit as a product of this unit and a number. This number is called the *numerical value* of the quantity expressed in this unit.

In formal treatments of quantities and units, this relation may be expressed in the form

$$A = \{A\} \cdot [A]$$

where A is the symbol for the physical quantity, $[A]$ the symbol for the unit and $\{A\}$ symbolizes the numerical value of the quantity A expressed in the unit $[A]$. For vectors and tensors the components are quantities which may be expressed as described above.

If a quantity is expressed in another unit which is k times the first unit, then the new numerical value becomes $1/k$ times the first numerical value; the physical quantity, which is the product of the numerical value and the unit, is thus independent of the unit.

REMARK ON NOTATION FOR NUMERICAL VALUES

It is essential to distinguish between the quantity itself and the numerical value of the quantity expressed in a particular unit. The numerical value of a quantity expressed in a particular unit could be indicated by placing braces (curly brackets) around the quantity symbol and using the unit as a subscript. It is, however, preferable to indicate the numerical value explicitly as the ratio of the quantity to the unit.

2.2 Quantities and equations**2.2.1 Mathematical operations with quantities**

Two or more physical quantities cannot be added or subtracted unless they belong to the same category of mutually comparable quantities.

Physical quantities are multiplied or divided by one another according to the rules of algebra; the product or the quotient of two quantities, A and B , satisfies the relations

$$AB = \{A\} \{B\} \cdot [A] [B]$$

Thus, the product $\{A\} \{B\}$ is the numerical value $\{AB\}$ of the quantity AB , and the product $[A] [B]$ is the unit $[AB]$ of the quantity AB . Similarly, the quotient $\{A\}/\{B\}$ is the numerical value $\{A/B\}$ of the quantity A/B , and the quotient $[A]/[B]$ is the unit $[A/B]$ of the quantity A/B .

2.2.2 Equations between quantities and equations between numerical values

Two types of equation are used in science and technology: *equations between quantities*, in which a letter symbol denotes the physical quantity (i.e. numerical value \times unit), and *equations between numerical values*. Equations between numerical values depend on the choice of units, whereas equations between quantities have the advantage of being independent of this choice. Therefore the use of equations between quantities should normally be preferred.

2.2.3 Empirical constants

An empirical relation is often expressed in the form of an equation between the numerical values of certain physical quantities. Such a relation depends on the units in which the various physical quantities are expressed.

An empirical relation between numerical values can be transformed into an equation between physical quantities, containing one or more empirical constants. Such an equation between physical quantities has the advantage that the form of the equation is independent of the choice of the units. The numerical values of the empirical constants occurring in such an equation depend, however, on the units in which they are expressed, as is the case with other physical quantities.

2.2.4 Numerical factors in quantity equations

Equations between quantities sometimes contain *numerical factors*. These numerical factors depend on the definitions chosen for the quantities occurring in the equations.

EXAMPLE

$$E_k = \frac{1}{2} mv^2$$

2.2.5 Systems of quantities and equations between quantities; base quantities and derived quantities

Physical quantities are related to one another through equations that express laws of nature or define new quantities.

For the purpose of defining unit systems and introducing the concept of dimensions, it is convenient to consider some quantities as mutually independent, i.e. to regard these as *base quantities*, in terms of which the other quantities can be defined or expressed by means of equations; the latter quantities are called *derived quantities*.

It is a matter of choice how many and which quantities are considered to be base quantities.

The whole set of physical quantities included in ISO 31 is considered as being founded on seven base quantities: **length L, mass M, time T, electric current I, thermodynamic temperature Θ , amount of substance N and luminous intensity J.**

In the field of mechanics a system of quantities and equations founded on three base quantities is generally used. In ISO 31-3, the base quantities used are length, mass and time.

In the field of electricity and magnetism a system of quantities and equations founded on four base quantities is generally used. In ISO 31-5, the base quantities used are length, mass, time and electric current.

In the same field, however, systems founded on only three base quantities, length, mass and time, in particular the "Gaussian" or symmetric system, have been widely used. (See ISO 31-5:1992, annex A.)

2.2.6 Dimension of a quantity

Any quantity Q can be expressed in terms of other quantities by means of an equation. The expression may consist of a sum of terms. Each of these terms can be expressed as a product of powers of base quantities A, B, C, \dots from a chosen set, sometimes multiplied by a numerical factor ξ , i.e. $\xi A^\alpha B^\beta C^\gamma \dots$, where the set of exponents $(\alpha, \beta, \gamma, \dots)$ is the same for each term.

The *dimension* of the quantity Q is then expressed by the dimensional product

$$\dim Q = A^\alpha B^\beta C^\gamma \dots$$

where A, B, C, \dots denote the dimensions of the base quantities A, B, C, \dots , and where $\alpha, \beta, \gamma, \dots$ are called the *dimensional exponents*.

A quantity all of whose dimensional exponents are equal to zero is often called a **dimensionless quantity**. Its dimensional product or dimension is $A^0 B^0 C^0 \dots = 1$. Such a quantity of **dimension one** is expressed as a number.

In the system founded on the seven base quantities length, mass, time, electric current, thermodynamic temperature, amount of substance and luminous intensity, the base dimensions may be denoted by L, M, T, I, O, N and J respectively and the dimension of a quantity Q becomes in general

$$\dim Q = L^a M^b T^c I^d O^e N^f J^g.$$

EXAMPLES

| Quantity | Dimension |
|------------------|----------------|
| velocity | LT^{-1} |
| angular velocity | T^{-1} |
| force | $LM T^{-2}$ |
| energy | $L^2 M T^{-2}$ |
| relative density | 1 |

2.3 Units

2.3.1 Coherent unit systems

Units might be chosen arbitrarily, but making an independent choice of a unit for each quantity would lead to the appearance of additional numerical factors in the equations between the numerical values.

It is possible, however, and in practice more convenient, to choose a system of units in such a way that the equations between numerical values have exactly the same form (including the numerical factors) as the corresponding equations between the quantities. A unit system defined in this way is called **coherent** with respect to the system of quantities and equations in question. The SI is such a system. The corresponding system of quantities is given in ISO 31-1 to ISO 31-10 and in ISO 31-12 and ISO 31-13.

For a particular system of quantities and equations, a coherent system of units is obtained by first defining units for the base quantities, the **base units**. Then for each derived quantity, the definition of the corresponding **derived unit** in terms of the base units is given by an algebraic expression obtained from the dimensional product (see 2.2.6) by replacing the symbols for the base dimensions by those of the base units. In particular, a quantity of dimension one acquires the unit 1. In such a coherent unit system no numerical factor other than the number 1 ever occurs in the expressions for the derived units in terms of the base units.

2.3.2 SI units and their decimal multiples and sub-multiples

The name *International System of Units* (Système International d'Unités), with the international abbreviation SI was adopted by the 11th

General Conference on Weights and Measures (Conférence Générale des Poids et Mesures, CGPM) in 1960.

This system includes

- base units
- derived units including supplementary units which together form the coherent system of *SI units*.

2.3.2.1 Base units

The seven base units are listed in Table 1.

Table 1 - SI base units

| Base quantity | SI base unit | |
|---------------------------|--------------|--------|
| | Name | Symbol |
| length | metre | m |
| mass | kilogram | kg |
| time | second | s |
| electric current | ampere | A |
| thermodynamic temperature | kelvin | K |
| amount of substance | mole | mol |
| luminous intensity | candela | cd |

2.3.2.2 Derived units including supplementary units

The expressions for the coherent derived units in terms of the base units can be obtained from the dimensional products by using the following formal substitutions:

$$\begin{array}{ll} L \rightarrow m & I \rightarrow A \\ M \rightarrow kg & \Theta \rightarrow K \\ T \rightarrow s & N \rightarrow mol \\ & J \rightarrow cd \end{array}$$

In 1960, the CGPM classified the SI units radian, rad, and steradian, sr, for plane angle and solid angle respectively as "supplementary units".

In 1980, the *International Committee for Weights and Measures* (Comité International des Poids et Mesures, CIPM) decided to interpret the class of supplementary units in the SI as a class of dimensionless derived units for which the CGPM allows the freedom of using or not using them in expressions for SI derived units.

Although, as a consequence of this interpretation, the coherent unit for plane angle and for solid angle is the number 1, it is convenient to use the special names radian, rad, and steradian, sr, instead of the number 1 in many practical cases.

Table 2 - SI derived units with special names, including SI supplementary units

| Derived quantity | SI derived unit | | |
|---|------------------------------|--------|--|
| | Special name | Symbol | Expressed in terms of SI base units and SI derived units |
| plane angle | radian | rad | 1 rad = 1 m/m = 1 |
| solid angle | steradian | sr | 1 sr = 1 m ² /m ² = 1 |
| frequency | hertz | Hz | 1 Hz = 1 s ⁻¹ |
| force | newton | N | 1 N = 1 kg · m/s ² |
| pressure, stress | pascal | Pa | 1 Pa = 1 N/m ² |
| energy, work, quantity of heat | joule | J | 1 J = 1 N · m |
| power, radiant flux | watt | W | 1 W = 1 J/s |
| electric charge, quantity of electricity | coulomb | C | 1 C = 1 A · s |
| electric potential, potential difference, tension, electromotive force | volt | V | 1 V = 1 W/A |
| capacitance | farad | F | 1 F = 1 C/V |
| electric resistance | ohm | Ω | 1 Ω = 1 V/A |
| electric conductance | siemens | S | 1 S = 1 Ω ⁻¹ |
| magnetic flux | weber | Wb | 1 Wb = 1 V · s |
| magnetic flux density | tesla | T | 1 T = 1 Wb/m ² |
| inductance | henry | H | 1 H = 1 Wb/A |
| Celsius temperature | degree Celsius ¹⁾ | °C | 1 °C = 1 K |
| luminous flux | lumen | lm | 1 lm = 1 cd · sr |
| illuminance | lux | lx | 1 lx = 1 lm/m ² |

1) Degree Celsius is a special name for the unit kelvin for use in stating values of Celsius temperature. (See also ISO 31-4:1992, items 4-1.a and 4-2.a.)

EXAMPLES

Quantity

Symbol for SI unit expressed in terms of the seven base units (and the supplementary units in some cases)

velocity
angular velocity
force
energy
relative density

m/s
rad/s or s⁻¹
kg · m/s²
kg · m²/s²
1

For some of the SI derived units, special names and symbols exist; those approved by the CGPM are listed in tables 2 (and 3).

It is often of advantage to use special names and symbols in compound expressions for units.

2.3.2.3 SI prefixes

In order to avoid large or small numerical values, decimal multiples and sub-multiples of the SI units are added to the coherent system within the framework of the SI. They are formed by means of the prefixes listed in Table 4.

Table 4 - SI prefixes

| Factor | Prefix | |
|------------|--------|--------|
| | Name | Symbol |
| 10^{24} | yotta | Y |
| 10^{21} | zetta | Z |
| 10^{18} | exa | E |
| 10^{15} | peta | P |
| 10^{12} | tera | T |
| 10^9 | giga | G |
| 10^6 | mega | M |
| 10^3 | kilo | k |
| 10^2 | hecto | h |
| 10 | deca | da |
| 10^{-1} | deci | d |
| 10^{-2} | centi | c |
| 10^{-3} | milli | m |
| 10^{-6} | micro | μ |
| 10^{-9} | nano | n |
| 10^{-12} | pico | p |
| 10^{-15} | femto | f |
| 10^{-18} | atto | a |
| 10^{-21} | zepto | z |
| 10^{-24} | yocto | y |

For information about the use of the prefixes, see 3.2.4.

The SI units and their decimal multiples and submultiples formed by use of the prefixes are specially recommended.

2.3.3 The unit one

The coherent SI unit for any quantity of dimension one is the unit one, symbol 1. It is generally not written out explicitly when such a quantity is expressed numerically.

EXAMPLE

Refractive index $n = 1,53 \times 1 = 1,53$

In the case of certain such quantities, however, the unit 1 has special names that could be used or not, depending on the context.

EXAMPLES

Plane angle $\alpha = 0,5 \text{ rad}$
 $= 0,5$,
 Solid angle $\Omega = 2,3 \text{ sr}$
 $= 2,3$

Decimal multiples and sub-multiples of the unit one are expressed by powers of 10. They shall not be expressed by combining the symbol 1 with a prefix.

In some cases the symbol % (per cent) is used for the number 0,01.

NOTES

3 In some countries the symbol ‰ ("per mill", or per thousand) is used for the number 0,001. This symbol should be avoided.

4 Since per cent and per mill are numbers it is in principle meaningless to speak about percentage by mass or percentage by volume. Additional information, such as % (m/m) or % (V/V), should not therefore be attached to the unit symbol. The preferred way of expressing a mass fraction is: "the mass fraction is 0,67" or "the mass fraction is 67 %", and the preferred way of expressing a volume fraction is: "the volume fraction is 0,75" or "the volume fraction is 75 %". Mass and volume fractions can also be expressed in the form $5 \mu\text{g/g}$ or $4,2 \text{ ml/m}^3$.

Abbreviations such as ppm, pphm and ppb shall not be used.

2.3.4 Other unit systems and miscellaneous units

The CGS system of mechanical units is a coherent system the base units of which are centimetre, gram and second for the three base quantities length, mass and time.

In practice this system was enlarged by adding the kelvin, the candela and the mole as base units for the base quantities thermodynamic temperature, luminous intensity and amount of substance.

Units used in electricity and magnetism have been defined in the CGS system in several ways depending on the system of quantities and equations chosen. The "Gaussian" or symmetric CGS system, coherent with the "Gaussian" or symmetric system of quantities and equations founded on three base quantities, has been widely used. For further information on this system, see ISO 31-5:1992, Annex A.

The special names and symbols for derived CGS units such as dyne, erg, poise, stokes, gauss, oersted and maxwell shall not be used together with the SI.

Table 5 - Units used with the SI

| Quantity | Unit | | |
|-------------|---------------------|--------------------|---|
| | Name | Symbol | Definition |
| time | minute | min | 1 min = 60 s |
| | hour | h | 1 h = 60 min |
| | day | d | 1 d = 24 h |
| plane angle | degree | ° | 1 ° = $(\pi/180)\text{rad}$ = $(\pi/180) \text{ rad}$ |
| | minute | ' | 1' = $(1/60)^\circ$ |
| | second | " | 1" = $(1/60)'$ |
| volume | litre | l, L ¹⁾ | 1 l = 1 dm ³ = 1 dm |
| mass | tonne ²⁾ | t | 1 t = 10 ³ kg |

¹⁾ The two symbols for litre are on an equal footing. The CIPM will, however, make a survey on the development

of the use of the two symbols in order to see if one of the two may be suppressed.

²⁾ Also called the metric ton in the English language.

Table 6 - Units used with the SI, whose values in SI units are obtained experimentally

| Quantity | Unit | | |
|----------|--------------------------|--------|---|
| | Name | Symbol | Definition |
| energy | electronvolt | eV | The electronvolt is the kinetic energy acquired by an electron in passing through a potential difference of 1 volt in vacuum: $1 \text{ eV} \approx 1,602\,177 \times 10^{-19} \text{ J}$. |
| mass | unified atomic mass unit | u | The unified atomic mass unit is equal to $(1/12)$ of the mass of an atom of the nuclide ^{12}C : $1 \text{ u} \approx 1,660\,540 \times 10^{-27} \text{ kg}$. |

In other parts of ISO 31, the special names for the derived CGS units are given in informative annexes which are not integral parts of the standards.

There are certain units outside the SI which are recognized by the CIPM as having to be retained for use together with the SI, e.g. minute, hour and electronvolt. These units are given in Tables 5 and 6.

Other coherent systems of units have been defined, e.g. a system based on the units foot, pound and second and a system based on the units metre, kilogram-force and second.

Apart from these, other units have been defined which do not belong to any coherent system, e.g. the atmosphere, the nautical mile and the curie.

3 Recommendations for printing symbols and numbers

3.1 Symbols for quantities

3.1.1 Symbols

The symbols for physical quantities are generally single letters of the Latin or Greek alphabet, sometimes with subscripts or other modifying signs. These **symbols** are printed in *italic* (sloping) type (irrespective of the type used in the rest of the text).

The symbol is not followed by a full stop except for normal punctuation, e.g. at the end of a sentence.

NOTES

5 Symbols for quantities are given in ISO 31-1 to ISO 31-10 and in ISO 31-12 and ISO 31-13.

6 Notations for vectorial and other non-scalar quantities are given in ISO 31-11, on mathematical signs and symbols.

7 Exceptionally, symbols made up of two letters are sometimes used for combinations of dimension one of quantities (e.g. Reynolds number, Re). If such a two-letter symbol appears as a factor in a product, it is recommended that it be separated from the other symbols.

3.1.2 Rules for the printing of subscripts

When, in a given context, different quantities have the same letter symbol or when, for one quantity, different applications or different values are of interest, a distinction can be made by use of subscripts.

The following principles for the printing of subscripts are recommended:

A subscript that represents a symbol for a physical quantity is printed in *italic* (sloping) type.

Other subscripts are printed in roman (upright) type.

EXAMPLES

Upright subscripts

C_g (g : gas)

g_n (n : normal)

μ_r (r : relative)

E_k (k : kinetic)

χ_e (e : electric)

$T_{1/2}$ ($1/2$: half)

Sloping subscripts

C_p (p : pressure)

$\sum_n a_n \delta_n$ (n : running number)

$\sum_x a_x b_x$ (x : running number)

g_{ik} (i, k : running numbers)

p_x (x : x -coordinate)

l_λ (λ : wavelength)

NOTES

8 Numbers as subscripts should be printed in roman (upright) type. However, letter symbols representing numbers are generally printed in *italic* (sloping) type.

3.1.3 Combination of symbols for quantities; elementary Operations with quantities

When symbols for quantities are combined in a product, this process of combination may be indicated in one of the following ways:

$$ab, a\,b, a \cdot b, a \times b$$

NOTES

10 In some fields, e.g. in vector analysis, distinction is made between $a \cdot b$ and $a \times b$.

11 For multiplication of numbers, see 3.3.3.

12 In systems with limited character sets a dot on the line may be used instead of a half-high dot.

Division of one quantity by another may be indicated in one of the following ways:

$$\frac{a}{b}, a/b \text{ or by writing the product of } a \text{ and } b^{-1},$$

e.g. $a \cdot b^{-1}$

3.2 Names and symbols for units

3.2.1 International symbols for units

When international symbols for units exist, they, and no other, shall be used. They shall be printed in roman (**upright**) type (irrespective of the type used in the rest of the text), shall remain unaltered in the plural shall be written without a final full stop (period) except for normal punctuation, e.g. at the end of a sentence.

Any attachment to a unit symbol as a means of giving information about the special nature of the quantity or context of measurement under consideration is incorrect.

EXAMPLE

$$U_{\max} = 500 \text{ V} \text{ (not } U = 500 \text{ V}_{\max}\text{)}$$

The unit symbols shall in general be printed in lower case letters except that the first letter is printed in upper case when the name of the unit is derived from a proper name.

EXAMPLES

| | |
|----|--------|
| m | metre |
| s | second |
| A | ampere |
| Wb | weber |

3.2.2 Combination of symbols for units

When a compound unit is formed by multiplication of two or more units, this should be indicated in one of the following ways:

$$\text{N}\cdot\text{m}, \quad \text{N m}$$

NOTES

13 In systems with limited character sets a dot on the line may be used instead of a half high dot.

14 The latter form may also be written without a space, provided that special care is taken when the symbol for one of the units is the same as the symbol for a prefix.

EXAMPLE

mN means millinewton, not metre newton.

When a compound unit is formed by dividing one unit by another, this should be indicated in one of the following ways:

$$\frac{\text{m}}{\text{s}} \quad \text{m/s} \quad \text{m}\cdot\text{s}^{-1}$$

A solidus (/) shall not be followed by a multiplication sign or a division sign on the same line unless parentheses are inserted to avoid any ambiguity. In complicated cases negative powers or parentheses shall be used.

3.2.3 Printing of symbols for units

No recommendation is made or implied about the font of upright type in which symbols for units are to be printed.

NOTE 15 In this series of publications the font used in such cases is generally that of the associated text, but this does not constitute a recommendation.

3.2.4 Printing and use of prefixes

Symbols for prefixes should be printed in roman (upright) type without a space between the symbol for the prefix and the symbol for the unit.

Compound prefixes shall not be used.

EXAMPLE

Write nm (nanometre) for 10^{-9} m, not mμm.

The symbol of a prefix is considered to be combined with the single unit symbol to which it is directly attached, forming with it a new symbol (for a decimal multiple or sub-multiple) which can be raised to a positive or negative power, and which can be combined with other unit symbols to form symbols for compound units (see 3.2.2).

EXAMPLES

$$\begin{aligned} 1 \text{ cm}^3 &= (10^{-2} \text{ m})^3 = 10^{-6} \text{ m}^3 \\ 1 \text{ } \mu\text{s}^{-1} &= (10^{-6} \text{ s})^{-1} = 10^6 \text{ s}^{-1} \\ 1 \text{ kA/m} &= (10^3 \text{ A})/\text{m} = 10^3 \text{ A/m} \end{aligned}$$

NOTE 16 For historical reasons the name of the base unit or mass, the kilogram, contains the name of the SI prefix, "kilo". Names of the decimal multiples and sub-multiples of the unit of mass are formed by adding the prefixes to the word „gram“, e.g. milligram (mg) instead of microkilogram (μkg).

3.3 Numbers

3.3.1 Printing of numbers

Numbers should generally be printed in roman (upright) type.

To facilitate the reading of numbers with many digits, these may be separated into suitable groups, preferably of three, counting from the decimal sign towards the left and the right; the groups should be separated by a small space, and never by a comma or a point, or by any other means.

3.3.2 Decimal sign

The decimal sign is a comma on the line.

If the magnitude of the number is less than unity, the decimal sign should be preceded by a zero.

NOTE 17 In documents in the English language, a dot is often used instead of a comma. If a dot is used, it should be on the line. In accordance with an ISO Council decision, the decimal sign is a comma in ISO documents.

3.3.3 Multiplication of numbers

The sign for multiplication of numbers is a cross (\times) or a dot half-high (\cdot).

NOTES

18 If a dot half-high is used as the multiplication sign, a comma should be used as the decimal sign. If a dot is used as the decimal sign, a cross should be used as the multiplication sign.

19. In ISO documents, the dot is not used directly between numbers to indicate multiplication.

3.4 Expressions for quantities

The symbol of the unit shall be placed after the numerical value in the expression for a quantity, leaving a space between the numerical value and the unit symbol. It should be noted that, in accordance with this rule, the symbol $^{\circ}\text{C}$ for degree Celsius shall be preceded by a space when expressing a Celsius temperature.

The only exceptions to this rule are for the units degree, minute and second for plane angle, in which case there shall be no space between the numerical value and the unit symbol.

If the quantity to be expressed is a sum or a difference of quantities then either parentheses shall be used to combine the numerical values, placing the common unit symbol after the complete numerical value, or the expression shall be written as the sum or difference of expressions for the quantities.

EXAMPLES

$$l = 12 \text{ m} - 7 \text{ m} = (12 - 7) \text{ m} = 5 \text{ m}$$

$$t = 28.4 \text{ }^{\circ}\text{C} \pm 0.2 \text{ }^{\circ}\text{C} = (28.4 \pm 0.2) \text{ }^{\circ}\text{C}$$

(not $28.4 \pm 0.2 \text{ }^{\circ}\text{C}$)

$$\lambda_{\text{e}} = 220 \times (1 \pm 0.02) \text{ W}/(\text{m}\cdot\text{K})$$

3.5 Symbols for chemical elements and nuclides

Symbols for chemical elements shall be written in roman (upright) type (irrespective of the type used in the rest of the text). The symbol is not followed by a full stop except for normal punctuation, e.g. at the end of a sentence.

EXAMPLES

H He C Ca

A complete list of the symbols for the chemical elements is given in ISO 31-8:1992, annex A, and ISO 31-9:1992, annex A.

The attached subscripts or superscripts specifying a nuclide or molecule shall have the following meanings and positions.

The nucleon number (mass number) of a nuclide is shown in the left superscript position, e.g.



The number of atoms of a nuclide in a molecule is shown in the right subscript position, e.g.



The proton number (atomic number) may be indicated in the left subscript position, e.g.



If necessary, a state of ionization or an excited state may be indicated in the right superscript position.

EXAMPLES

| | |
|---------------------------|--|
| State of ionization: | Na^+ |
| | PO_4^{3-} or $(\text{PO}_4)^{3-}$ |
| Electronic excited state: | He^* , N0^* |
| Nuclear excited state: | $^{110}\text{Ag}^*$, $^{110}\text{Ag}^{\text{m}}$ |

3.6 Mathematical signs and symbols

Mathematical signs and symbols recommended for use in the physical sciences and technology are given in ISO 31-11.

3.7 Greek alphabet (upright and sloping types)

| | | | | |
|---------|-----------|---------------------|-----------|---------------------|
| alpha | Λ | α | A | a |
| beta | B | β | B | β |
| gamma | Γ | γ | Γ | γ |
| delta | Δ | δ | Δ | δ |
| epsilon | E | ε | E | ε |
| zeta | Z | ζ | Z | ζ |
| eta | H | η | H | η |
| theta | Θ | θ, ϑ | Θ | θ, ϑ |
| iota | I | ι | I | ι |
| kappa | K | κ | K | κ |
| lambda | Λ | λ | Λ | λ |
| mu | M | μ | M | μ |
| nu | N | ν | N | ν |
| xi | Ξ | ξ | Ξ | ξ |
| omicron | O | o | O | o |
| π | Π | π | Π | π |
| rho | P | ρ | P | $\rho,$ |
| sigma | Σ | σ | Σ | σ |
| tau | T | τ | T | τ |
| upsilon | Y | υ | Y | υ |
| phi | Φ | ϕ | Φ | ϕ |
| chi | X | χ | X | χ |
| psi | Ψ | ψ | Ψ | ψ |
| omega | Ω | ω | Ω | ω |

5.2 Computer Symbols

Wherever possible the symbols in the second column of the tables have been chosen so that their meaning is readily apparent. They have been constructed from the CCITT International Telegraph Alphabet, restricted character set. They are therefore suitable for use in a wide range of situations e. g.: Telex messages, letters, computer printouts etc.

To ensure that the symbols can be used in a wide range of programming languages they currently have been kept to less than six characters long. The symbols should be used as defined, and, in accordance with modern programming practice, should have their type explicitly declared before use. The following rules were applied in the derivation of the symbols:

1. Only upper case letter A - Z and digits 0 - 9 have been used.
2. Formerly Greek letters have been spelled out, if necessary in abbreviated form or with changed spelling. This practice is considered obsolete.

3. The Froude 'circular' symbols are defined by the prefix CIRC.
4. All symbols start with a letter.
5. Qualifiers and operators, preferably two characters, are currently suffixed to the main symbol line, without spacing.
6. No one computer compatible symbol should be used for different concepts in a given context. This goal has not been completely achieved for the whole list. Ad hoc solutions have been attempted but discarded as unsatisfactory.
7. Since the computer compatible symbols have been proposed as the basis of attribute names for data exchanges, the above rules will probably be further developed in the near future.

A final remark on the Computer Symbols: in the computer, the letter O and figure 0 (zero) have fundamentally different meanings, but owing to their resemblance they can be easily confused. Thus it is necessary to distinguish rigorously between them. As a matter of fact there are contradictory conventions being widely used.

5.3 Documentation

5.3.1 ITTC Documents

1. International Towing Tank Conference, Standard Symbols 1971, BSRA Technical Memorandum No.400, August 1971.
2. International Towing Tank Conference, Standard Symbols 1976. BSRA T.M. No.500, 1976.
3. ITTC Dictionary of Ship Hydrodynamics. RINA Maritime Technology Monograph No.6, 1978.
4. Translation of Overall Index of Titles of Dictionary of Ship Hydrodynamics., Vol. 1: CETENA, Genova, 1984, Vol. 2: University of Tokyo, 1984.
5. Bibliography and Proposed Symbols on Hydrodynamic Technology as Related Model Tests of High Speed Marine Vehicles. Prep. by 17th ITTC High-Speed Marine Vehicle Committee. SPPA Maritime Research and Consulting. Rep. No.101, 1984.

5.3.2 Translations

A number of translations of the List of ITTC Standard Symbols into languages other than English have been made including French, German, Italian, Japanese, Russian, Spanish and Chinese. For obvious reasons these translations are no longer up-to-date as the present accepted list in English and the Russian one.

1. French Translation of ITTC Standard Symbols 1971., Association Francaise de Normalisation (AFNOR).
2. International vereinbarte Buchstabensymbole und Bezeichnungen auf dem Gebiet der Schiffshydrodynamik. Collatz, G. Schiff und Hafen 27 (1975) No.10.
3. Italian Translation of ITTC Standard Symbols 1971. Luise E. Appendix II, Report of Presentation Committee. Proceedings 14th ITTC, Vol. 4, Ottawa 1975.

4. Japanese Translation of ITTC Standard Symbols. Transactions of the Society of Naval Architects of Japan, No.538, April 1974.
5. Russian Translation of ITTC Standard Symbols 1971. Brodarski Institute Publication No.28, Zagreb 1974.
6. Simbolos Internacionales en Arquitectura Naval. Asociacion de Investigacion de la Construcccion Naval, Publication 7/75, Juli 1975, Madrid.
7. Report of Information Committee, Proc. 17th ITTC, Göteborg 1984.
8. Chinese Translation of ITTC Standard Symbols. China Ship Scientific Research Centre, Wuxi.

5.3.3 Other References

Apart from the organizations represented on the ITTC these symbols have been recommended for use in technical writing on naval architecture by a number of organizations concerned with marine matters including The Royal Institution of Naval Architects, the American Society of Naval Architects and Marine Engineers and the American, British, Canadian, Australian, and Italian Navies. Where possible, the symbols for Section 3.4.1, Waves are consistent with the IAHR/PIANC List of Sea State Parameters, Supplement to Bulletin No 52, January 1986.

In 1985 the Draught International Standard ISO/DIS 7463 Shipbuilding - Symbols for Computer Applications - has been published. The symbols are based on the list approved by the ITTC in Ottawa 1975 and a related list produced by the ISSC in 1974, inconsistencies having been removed. The ISO/TC8/SC15 has been notified that major changes of the ITTC Symbols are under discussion. Subsequently processing of ISO/DIS 7463 has not been postponed, but the standard has been published as ISO 7463 in 1990.